

The Runge-Kutta method

Advanced Numerics Seminar

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Outline

- View of LMK-Dynamics, -Numerics
- Time-splitting schemes
 - General remarks
 - Runge-Kutta + Advection
 - Sound-Advection-Buoyancy-System
 - Idealized tests
 - Implicit Vertical Advection
- Coupling Dynamics and Physics
- Dynamic Lower Boundary Condition

LMK - Dynamics

- Model equations: non-hydrostatic, full compressible, advection form
- Base state: hydrostatic
- Prognostic variables: cartesian wind components u , v , w
pressure perturbation p' , Temperature T (or $T' = T - T_0$)
humidity var. q_v , q_c , q_i , q_r , q_s , q_g
TKE
- Coordinate systems: rotated geographical coordinates
generalized terrain-following height coordinate
user-defined vertical stretching

Open questions:

- use shallow or deep atmospheric equations?
i.e. are terms $\sim w$ in advection earth curvature and Coriolis force important?
(diploma thesis) (e.g. Staniforth, Wood, 2003)
- diabatic terms in p-equation? (lecture H. Herzog)

Equation system of LM/LMK in spherical coordinates

$$\frac{\partial u}{\partial t} + \mathbf{v} \cdot \nabla u - \frac{\tan \phi}{r} uv + \frac{1}{r} uw = -\frac{1}{\rho r \cos \phi} \frac{\partial p}{\partial \lambda} + 2\Omega(v \sin \phi - w \cos \phi) + M_u$$

$$\frac{\partial v}{\partial t} + \mathbf{v} \cdot \nabla v + \frac{\tan \phi}{r} u^2 + \frac{1}{r} vw = -\frac{1}{\rho r} \frac{\partial p}{\partial \phi} - 2\Omega u \sin \phi + M_v$$

$$\frac{\partial w}{\partial t} + \mathbf{v} \cdot \nabla w - \frac{u^2 + v^2}{r} = -\frac{1}{\rho} \frac{\partial p}{\partial r} - g + 2\Omega u \cos \phi + M_w$$

$$\frac{\partial p}{\partial t} + \mathbf{v} \cdot \nabla p = -\frac{c_p}{c_v} p \nabla \cdot \mathbf{v}$$

$$\frac{\partial T}{\partial t} + \mathbf{v} \cdot \nabla T = -\frac{1}{\rho c_v} p \nabla \cdot \mathbf{v} + \frac{1}{\rho c_p} (Q_{ph} + M_T - \nabla \cdot \mathbf{R})$$

$$\rho \frac{\partial q_x}{\partial t} + \rho \mathbf{v} \cdot \nabla q_x = -\nabla \cdot \mathbf{P}_x - \nabla \cdot \mathbf{F}_x - I_x, \quad (x = v, c, i, r, s, g)$$

$$p = \rho R_d (1 + (R_v/R_d - 1)q_v - q_c - q_r - q_s - q_i - q_g)T$$

additionally:

- introduce a hydrostatic, steady base state
- Transformation to terrain-following coordinates
- shallow/deep atmosphere

Numerics

	LM	LMK
Grid	horizontal: Arakawa-C vertical: Lorenz	
Time integration	3-timelevels: Leapfrog	2-timelevels: Runge-Kutta 2. order, 3. order, <u>3. order TVD</u>
Advection u, v, w, T, p'	horizontal: centered diff. 2. order vertical: implicit 2. order	horizontal: upwind 3., <u>5. order</u> centered diff. 4., 6. order vertical: implicit 2. order implicit 3. order
Advection $q_v, q_c, q_i, q_r, \dots, TKE$	q_v, q_c : centered diff. 2. order q_i : Lin, Rood q_r, q_s : Semi-Lagrange (trilin.)	Bott-2, conservation form or Semi-Lagrange, tricubic/trilin.
Smoothing	Divergence damping	
	4. order diffusion	4. order diffusion ?
	Asselin-filtering	

Time scales of atmospheric processes

Process		char. velocity, ...	char. time (dx ~ 3 km or dz ~ 30 m)	type
Dynamics	Advection, horiz.	0...10...100 m/s	∞ ...300...30 s	slow
	vert.	0...30 m/s	∞ ...1 s	(implicit)
	Sound, horiz.	330 m/s	10 s	fast
	vert.	330 m/s	0.1 s	(implicit)
	Buoyancy		100 s (=1/N)	(slow)
Gravity waves, horiz.	0...200 m/s	∞ ...15 s	fast	
Coriolis		10000 s (=1/f)	slow	
Physics	Diffusion, vert.	0...10...100 m ² /s	∞ ...100 s ... 10 s	(implicit)
	Sedimentation, vert.	~5 m/s	6 s	(implicit)
			

--> weak stiffness in compressible models

Time integration methods

$$\frac{\partial q}{\partial t} = \mathcal{P}_s q + \mathcal{P}_f q$$

time splitting ratio:
 $n_s = DT / Dt$

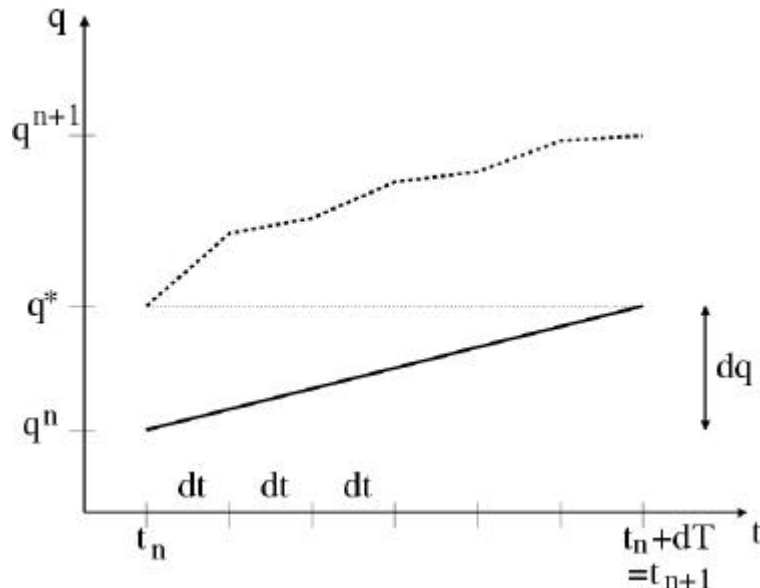
- Integration with small time step Δt (and e.g. additive splitting)
inefficient, interest only in slow processes
- Semi-implicit method (<-> Semi-Lagrange-Method)
- Time-splitting method
 - main reason: fast processes are computationally ,cheap‘
 - Additive splitting
 - partial operator splitting
Klemp, Wilhelmson (1978), Wicker, Skamarock, (1998, 2002), ...

Additive splitting

(complete operator splitting, method of fractional steps, multiplicative splitting)

Peaceman, Rachford (1955) (ADI-method), Marchuk (1974)

$$q^* = Q_s(q^t)$$
$$q^{t+\Delta T} = Q_f(Q_f(\dots Q_f(q^*)\dots))$$



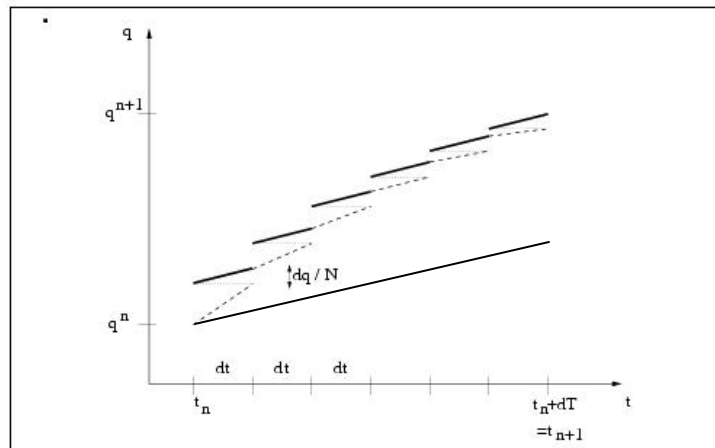
- costs: $1 * Q_s, n_s * Q_f$
- stability is guaranteed only if P_s and P_f both are stable *and* commutable (Leveque and Olinger, 1983)
- noisy \leftarrow only weak coupling between modes (Purser, Leslie, 1991)
- of 1. order in ΔT (for non-commutable operators)

extension: Strang (1968) for non-commutable operators 2. order:

$$q^{t+\Delta T} = (Q_f)^{n/2} Q_s (Q_f)^{n/2} q^t$$

\Rightarrow 2. order in ΔT

Time-splitted Euler-forward step (partial operator splitting)



$$q^* = Q_s(q^t), \quad dq_s = \frac{q^* - q^t}{\Delta T}$$

and

$$\begin{aligned} q^{t+\Delta t} &= Q_f(q^t) + \Delta t dq_s \\ q^{t+2\Delta t} &= Q_f(q^{t+\Delta t}) + \Delta t dq_s \\ &\dots \\ q^{t+\Delta T} &= Q_f(q^{t+(n_s-1)\Delta t}) + \Delta t dq_s \end{aligned}$$

- 2-timelevel scheme
- costs: $1 \times P_s$, $n_s \times P_f$
- Skamarock, Klemp (1992), MWR: scheme is not stable (but analysis only in the time domain)
- scheme can be stabilized by divergence filtering (Baldauf (2002), COSMO-Newsletter)

Time-integration scheme

- method of lines (semi-discretization)
- time-splitted Euler-forward step can be put into arbitrary ODE-solver

ODE-solvers:

explicit 2-timelevel schemes

- single stage: Euler method = forward differencing = Runge-Kutta 1. order
- multistage: Runge-Kutta 2. order (e.g. Heun method, midpoint method)
- Runge-Kutta 3. order

...

implicit 2-timelevel schemes

- single stage: backward differencing
- trapezoidal method = Crank-Nicholson

explicit 3-timelevel schemes *(occurrence of computational modes)*

- Leapfrog scheme
- Adams-Bashforth 2. order
- Magazenkov (1980)

...

but in practice: stability constraints

Klemp-Wilhelmson-time-splitting, Leapfrog-method

Klemp, Wilhelmson (1978), JAS

Leapfrog-scheme for ODE $dq/dt = f(q)$:

$$q^{n+1} = q^{n-1} + 2\Delta T f(q^n)$$

Leapfrog-scheme combined with splitting idea:

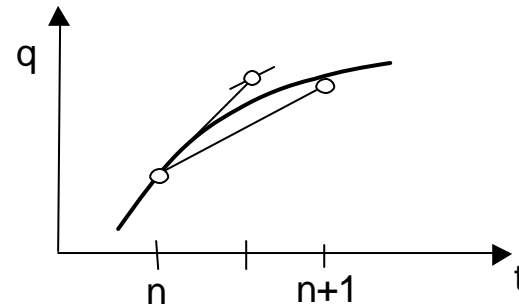
1. calculate the tendency of slow processes with q^t
 2. perform a KW-Euler-forward-splitting from $t - \Delta T$ to $t + \Delta T$ with this slow tendency
- 3-timelevel scheme
 - costs: $1 \times P_s, 2n_s \times P_f$
 - disadv.: only special advection schemes are applicable
 - scheme is stable with (weak) Asselin-filter and divergence damping (Skamarock and Klemp, 1992)

Time-splitting with Runge-Kutta 2. order

Wicker, Skamarock (1998), MWR

RK2-scheme (midpoint-method) for an ODE: $dq/dt=f(q)$

$$q^* = q^n + \frac{\Delta T}{2} f(q^n)$$
$$q^{n+1} = q^n + \Delta T f(q^*)$$



- 2-timelevel scheme
- Wicker, Skamarock (2002): upwind-advection stable: 3. order ($C < 0.88$)
- combined with time-splitting-idea:
'costs': 2^* slow process, $1.5 n_s^*$ fast process

'shortened RK2 version': first RK-step only with fast processes (Gassmann, 2004)

Runge-Kutta-Methods, order

order	number of free parameters	
1	0	Euler-forward
2	1	e.g. Heun, midpoint method
3	2	
4	2	
...	...	

general theory: Butcher (1964, ...), Butcher (1987) \Rightarrow

Runge-Kutta methods of 1. to 3. order: have the same order
for a single scalar equation and for a system of equations

Runge Kutta methods of order >4 : can have lower order for
systems of equations than for a single equation

3. order Runge-Kutta-schemes

$$\begin{aligned}k_1 &= f(t^n, y^n), \\k_2 &= f(t^n + \Delta t \cdot \alpha_2, y^n + \Delta t \cdot \beta_{21}k_1), \\k_3 &= f(t^n + \Delta t \cdot \alpha_3, y^n + \Delta t \cdot (\beta_{31}k_1 + \beta_{32}k_2)), \\y^{n+1} &= y^n + \Delta t \cdot (b_1k_1 + b_2k_2 + b_3k_3)\end{aligned}$$

Butcher-tableau:

0			
α_2	β_{21}		
α_3	β_{31}	β_{32}	
	b_1	b_2	b_3

6 conditions to generate a 3. order scheme:

$$\begin{aligned}b_1 + b_2 + b_3 &= 1 \\ \beta_{21} &= \alpha_2 \\ \beta_{31} + \beta_{32} &= \alpha_3 \\ b_2\alpha_2 + b_3\alpha_3 &= 1/2 \\ b_2\alpha_2^2 + b_3\alpha_3^2 &= 1/3 \\ b_3\alpha_2\beta_{32} &= 1/6\end{aligned}$$

RK3-Variants:

- TVD-RK3 (Shu, Osher, 1988), RK3b (Hundsdoerfer et al., 1995)

$$\begin{aligned}y^* &= y^n + \Delta t f(t^n, y^n), \\y^{**} &= \frac{3}{4}y^n + \frac{1}{4}y^* + \frac{1}{4}\Delta t f(t^n + \Delta t, y^*) \\y^{n+1} &= \frac{1}{3}y^n + \frac{2}{3}y^{**} + \frac{2}{3}\Delta t f(t^n + \frac{1}{2}\Delta t, y^{**})\end{aligned}$$

is used in LMK
(Förstner, Doms, 2004)

- RK3a (Hundsdoerfer et al., 1995)
- minimal storage scheme (Williamson, 1980)

-
- Wicker, Skamarock (2002) is *not* a 3. order RK-scheme

$$\begin{aligned}y^* &= y^n + \frac{1}{3}\Delta t f(t^n, y^n), \\y^{**} &= y^n + \frac{1}{2}\Delta t f(t^n + \frac{1}{3}\Delta t, y^*) \\y^{n+1} &= y^n + \Delta t f(t^n + \frac{1}{2}\Delta t, y^{**})\end{aligned}$$

Advection-schemes of higher order

$$\frac{q_i^{n+1} - q_i^n}{\Delta t} = -\frac{F_{i+1/2}^n - F_{i-1/2}^n}{\Delta x}$$

Fluxes of 3rd to 6th order (from spatial discretization of advection operator)

$$F_{i-1/2}^{(3)} = F_{i-1/2}^{(4)} - \frac{|u_{i-1/2}|}{12} (3(q_i - q_{i-1}) - (q_{i+1} - q_{i-2}))$$

$$F_{i-1/2}^{(4)} = \frac{u_{i-1/2}}{12} (7(q_i + q_{i-1}) - (q_{i+1} + q_{i-2}))$$

$$F_{i-1/2}^{(5)} = F_{i-1/2}^{(6)} - \frac{|u_{i-1/2}|}{60} (10(q_i - q_{i-1}) - 5(q_{i+1} - q_{i-2}) + (q_{i+2} - q_{i-3}))$$

$$F_{i-1/2}^{(6)} = \frac{u_{i-1/2}}{60} (37(q_i + q_{i-1}) - 8(q_{i+1} + q_{i-2}) + (q_{i+2} + q_{i-3}))$$

- Hundsdorfer et al. (1995), JCP
- Wicker, Skamarock (2002), MWR

stable Courant-numbers for advection schemes (Wicker, Skamarock, 2002)

	1.	2.	3.	4.	5.	6.
Leapfrog	0	1	0	0.72	0	0.62
Euler	1	0	0	0	0	0
RK2	1	0	0.87	0	0!	0
RK3	1.25	1.73	1.62	1.26	1.43	1.09
RK4	1.39	2.82	1.74	2.06	1.73	1.78

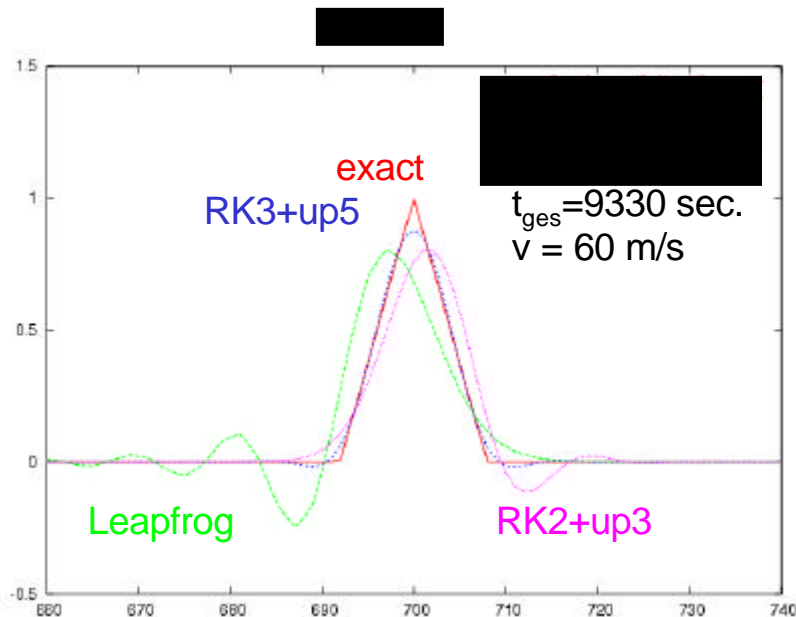
All 2. order Runge-Kutta-schemes have the same linear stability properties for $c=\text{const.}$!

All 3. order Runge-Kutta-schemes have the same linear stability properties for $c=\text{const.}$!

(holds also for Wicker, Skamarock (2002) ,RK3'-variant !)

Horizontal advection in time splitting schemes

- Leapfrog + centered diff. 2. order (currently used LM/LME) ($C < 1$)
 - Runge-Kutta 2. order $O(\Delta t^2)$ + upwind 3. order $O(\Delta x^3)$ ($C < 0.87$)
 - Runge-Kutta 3. order $O(\Delta t^3)$ + upwind 5. order $O(\Delta x^5)$ ($C < 1.43$)
- (Wicker, Skamarock, 2002)



advection equation

$$\frac{\partial f}{\partial t} + v \frac{\partial f}{\partial x} = 0$$

Courant number $C = v * \Delta t / \Delta x$

Von-Neumann stability analysis

Linearized PDE-system for $u(x,z,t)$, $w(x,z,t)$, ... with constant coefficients

Discretization u_{jl}^n , w_{jl}^n , ... (grid sizes Δx , Δz)

single Fourier-Mode:

$$u_{jl}^n = u^n \exp(i k_x j \Delta x + i k_z l \Delta z)$$

2-timelevel schemes:

$$\begin{pmatrix} u^{n+1} \\ w^{n+1} \\ p'^{n+1} \\ T'^{n+1} \end{pmatrix} = Q \begin{pmatrix} u^n \\ w^n \\ p'^n \\ T'^n \end{pmatrix}$$

Determine eigenvalues λ_i of Q

scheme is stable, if $\max_i |\lambda_i| \leq 1$

find λ_i analytically or numerically by scanning $k_x \Delta x = -\pi \dots + \pi$, $k_z \Delta z = -\pi \dots + \pi$

Sound

$$\frac{u^{n+1} - u^n}{\Delta t} = -\frac{1}{\rho_0} (\beta_1^s \delta_x p'^{n+1} + (1 - \beta_1^s) \delta_x p'^n)$$

$$\frac{w^{n+1} - w^n}{\Delta t} = -\frac{1}{\rho_0} (\beta_2^s \delta_z p'^{n+1} + (1 - \beta_2^s) \delta_z p'^n)$$

$$\frac{p^{n+1} - p^n}{\Delta t} = -\frac{c_p}{c_v} p_0 (\beta_3^s \delta_x u^{n+1} + (1 - \beta_3^s) \delta_x u^n + \beta_4^s \delta_z w^{n+1} + (1 - \beta_4^s) \delta_z w^n)$$

$$\frac{T^{n+1} - T^n}{\Delta t} = -\frac{R}{c_v} T_0 (\beta_5^s \delta_x u^{n+1} + (1 - \beta_5^s) \delta_x u^n + \beta_6^s \delta_z w^{n+1} + (1 - \beta_6^s) \delta_z w^n)$$

- temporal discret.: 'generalized' Crank-Nicholson
 $\beta=1$: implicit, $\beta=0$: explicit
- spatial discret.: centered diff.

Courant-numbers: $C_{snd,x} = c_s \frac{\Delta t}{\Delta x}$, $C_{snd,z} = c_s \frac{\Delta t}{\Delta z}$, $c_s^2 = \frac{c_p}{c_v} \frac{p_0}{\rho_0}$

fully explicit	uncond. unstable	-	
forward-backward (Mesinger, 1977), unstaggered grid	stable for $C_x^2 + C_z^2 < 2$	neutral	4 dx, 4dz
forward-backward, staggered grid	stable for $C_x^2 + C_z^2 < 1$	neutral	2 dx, 2dz
forward-backw.+vertically Crank-Nic. ($\beta_{2,4,6}=1/2$)	stable for $C_x < 1$	neutral	2 dx
forward-backw.+vertically Crank-Nic. ($\beta_{2,4,6}>1/2$)	stable for $C_x < 1$	damping	2 dx

Divergence damping

$$\frac{\partial \mathbf{v}}{\partial t} + \dots = \dots + \alpha_{div} \nabla(\operatorname{div} \mathbf{v})$$

⇒ Diffusion of Divergence

Courant-numbers: $C_{div,x} := \alpha_{div} \frac{\Delta t}{\Delta x^2}, \quad C_{div,z} := \alpha_{div} \frac{\Delta t}{\Delta z^2}$

1D, explicit	stable for $C_{div,x} < \frac{1}{2}$
2D, explicit (staggered grid)	stable for $C_{div,x} + C_{div,z} < \frac{1}{2}$
2D, implicit	unconditionally stable
2D, vertically implicit	stable for $C_{div,x} < \frac{1}{2}, C_{div,z}$ arbitr.

Wicker, Skamarock (2002): $\alpha_{div} \approx 0.1 c_s^2 \Delta t \Rightarrow$ for LMK: $\alpha_{div} \approx 50000 m^2/s$

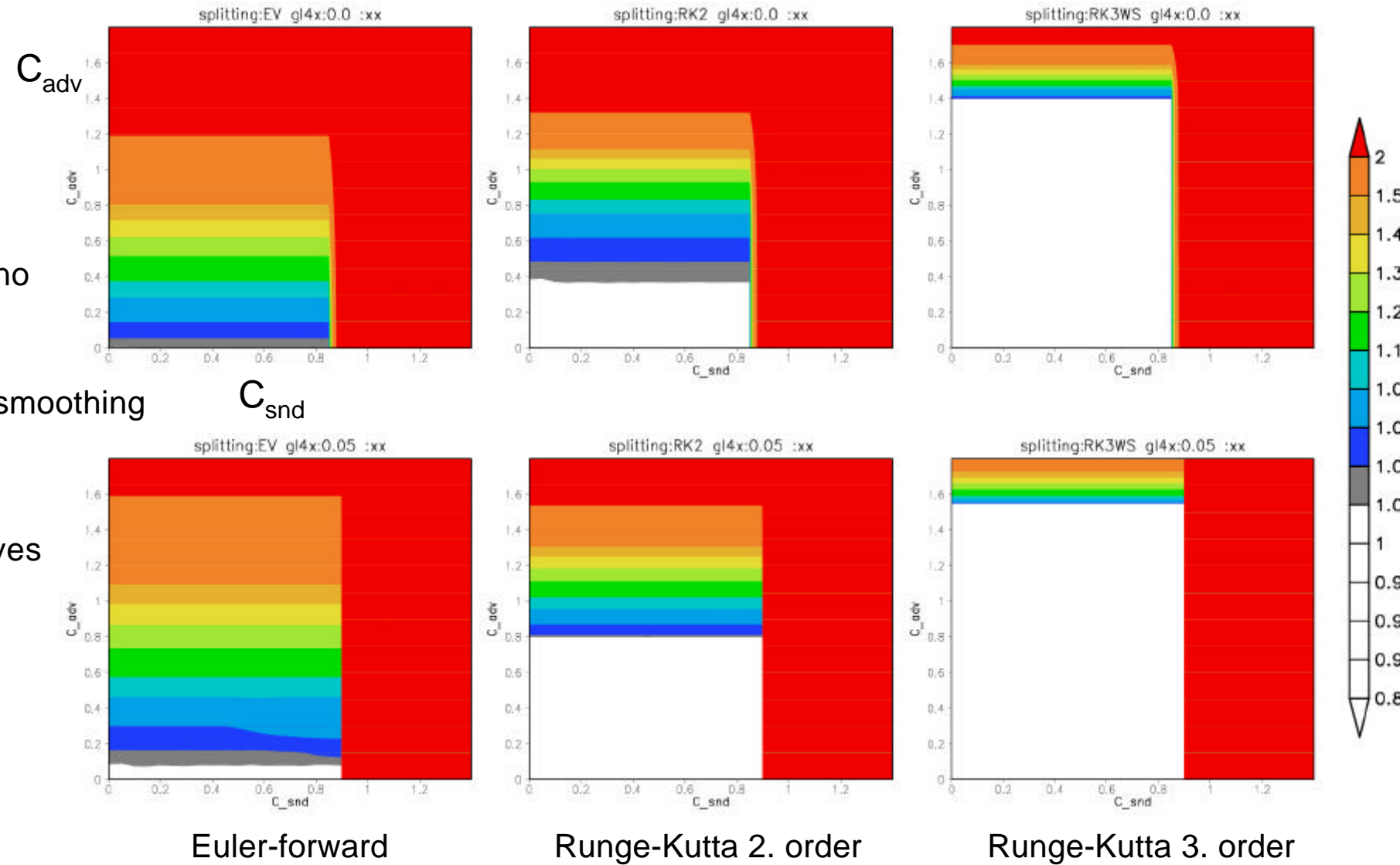
What is the influence of

- **different time-splitting schemes**
 - Euler-forward
 - Runge-Kutta 2. order
 - Runge-Kutta 3. order (WS2002)
- **and smoothing** (4. order horizontal diffusion) ?
 - $K_{\text{smooth}} \Delta t / \Delta x^4 = 0 / 0.05$

- fast processes (with operatorsplitting)
 - sound (Crank-Nic., $\beta=0.6$),
 - divergence-damping (vertical implicit, $C_{\text{div}}=0.1$)
 - no buoyancy
- slow process: upwind 5. order
- aspect ratio: $\Delta x / \Delta z=10$
- $\Delta T / \Delta t=12$

Deutscher Wetterdienst

Aktionsprogramm 2003

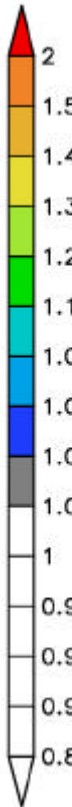
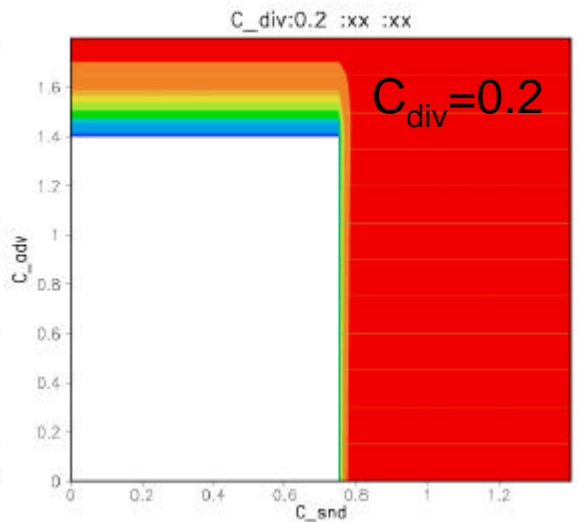
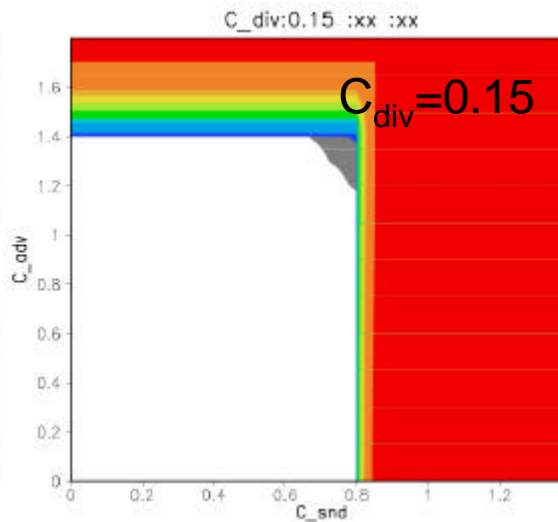
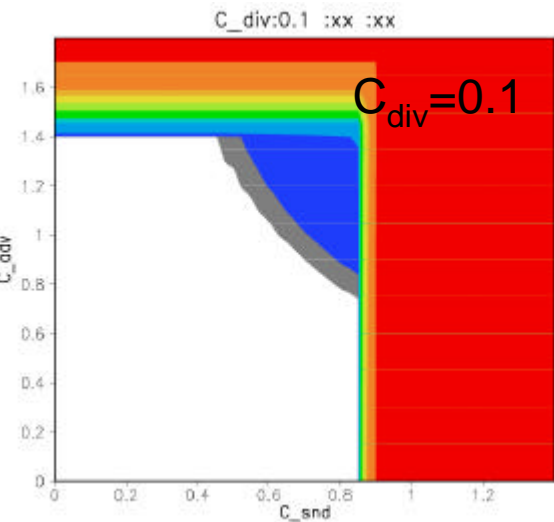
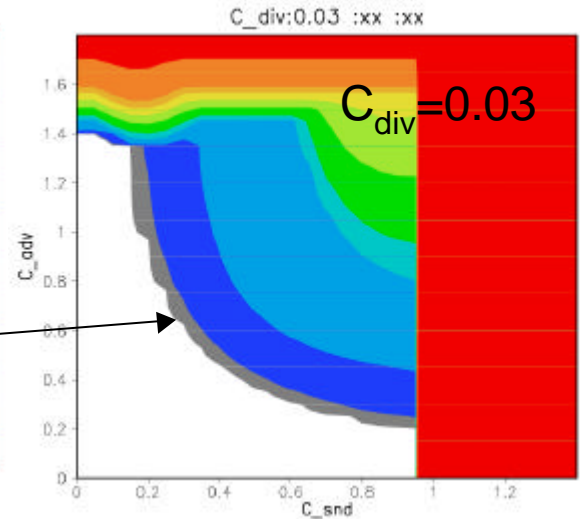
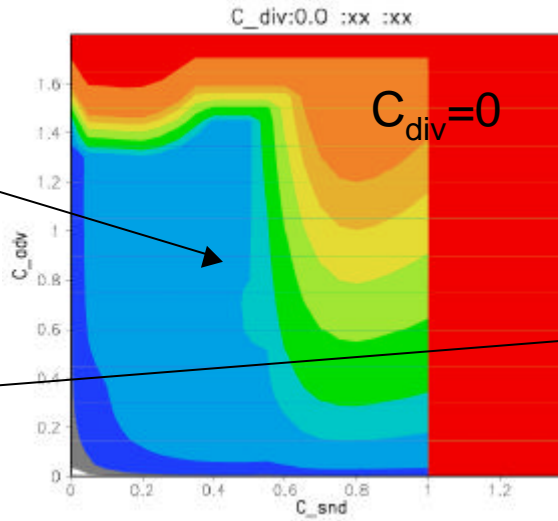


What is the influence of divergence filtering ?

- fast processes (operatorsplitting):
 - sound (Crank-Nic., $\beta=0.6$),
 - divergence damping (vertical implicit)
 - no buoyancy
- slow process: upwind 5. order
- time splitting RK 3. order (WS2002-Version)
- aspect ratio: $\Delta x / \Delta z=10$
- $\Delta T / \Delta t=6$

instability by purely horizontally propagating waves

stability limit by long waves ($k \rightarrow 0$)



Buoyancy terms:

$$\frac{w^{n+1} - w^n}{\Delta t} = g \left(\beta_T^b \frac{T'^{n+1}}{T_0} + (1 - \beta_T^b) \frac{T'^n}{T_0} - \beta_p^b \frac{p'^{n+1}}{p_0} - (1 - \beta_p^b) \frac{p'^n}{p_0} \right)$$

$$\frac{p'^{n+1} - p'^n}{\Delta t} = \rho_0 g (\beta_3^b w^{n+1} + (1 - \beta_3^b) w^n)$$

$$\frac{T'^{n+1} - T'^n}{\Delta t} = -\frac{\partial T_0}{\partial z} (\beta_4^b w^{n+1} + (1 - \beta_4^b) w^n)$$

acoustic cut-off frequency $\omega_a := \sqrt{N^2 + \frac{g^2}{c_s^2}}$; $C_{buoy} := \omega_a \Delta t$

$$C_\beta = \frac{1}{T_0} \frac{\partial T_0}{\partial z} \frac{c_s^2}{g} \approx -0.24 \text{ (standard atmosphere)}$$

fully explicit	unstable	-
forward-backward	stable for $C_{buoy} < 2$	neutral
Crank-Nicholson $\beta = 1/2$	uncond. stable	neutral
Crank-Nicholson $\beta > 1/2$	uncond. stable	damping
implicit	uncond. stable	damping

Commutation with other numerical operators:

$$Q_{buoy} \cdot Q_{sound} \neq Q_{sound} \cdot Q_{buoy}, \quad Q_{buoy} \cdot Q_{div} \neq Q_{div} \cdot Q_{buoy}$$

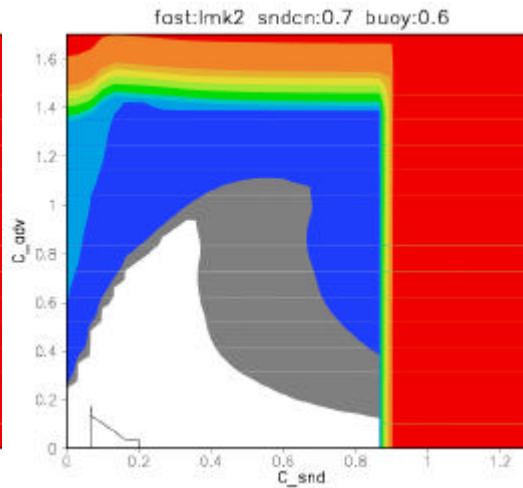
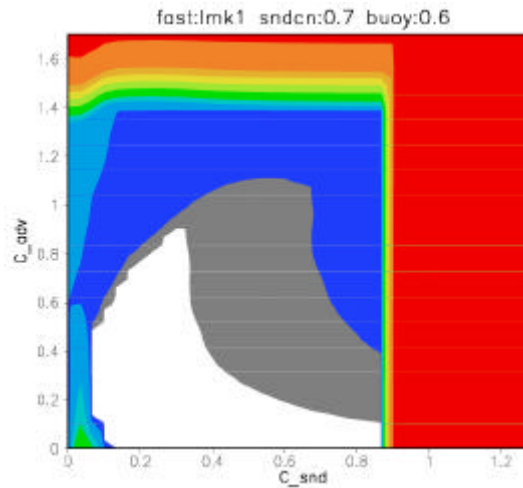
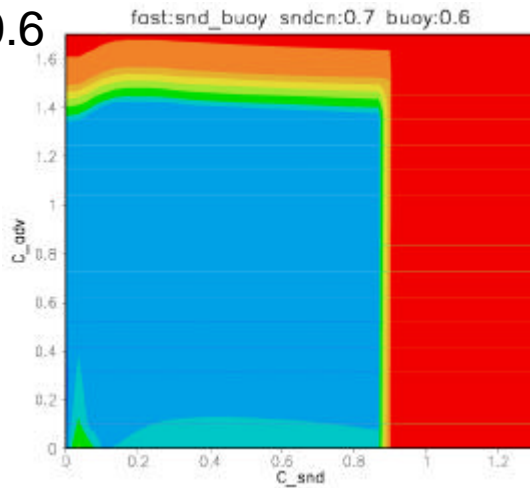
How to handle the fast processes with buoyancy?

with buoyancy ($C_{\text{buoy}} = \omega_a dt = 0.15$, standard atmosphere)

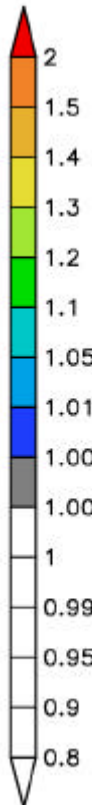
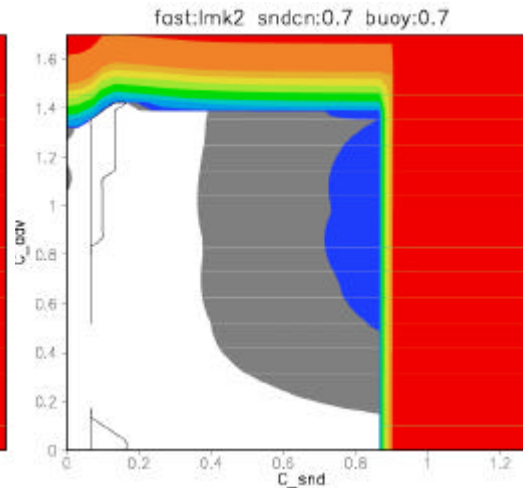
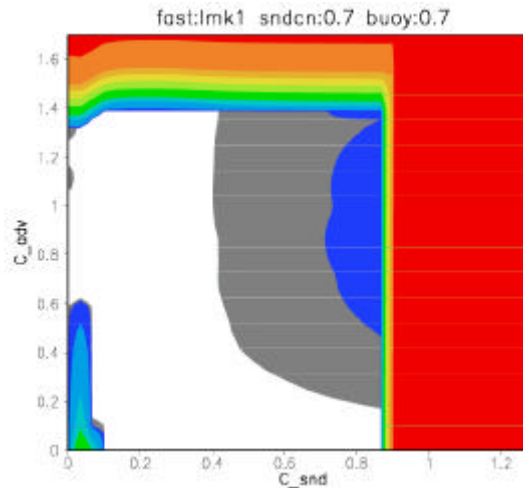
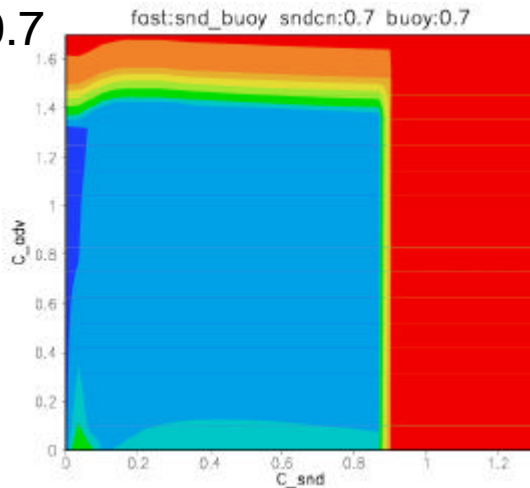
- different fast processes:
 - operatorsplitting (Marchuk-Splitting): 'Sound -> Div. -> Buoyancy'
 - partial adding of tendencies: '(Sound+Buoyancy) -> Div.'
 - adding of all fast tendencies: 'Sound+Div.+Buoyancy'
- different Crank-Nicholson-weights for buoyancy:
 $\beta = 0.6 / 0.7$

- RK3-scheme
- slow process: upwind 5. order
- aspect ratio: $dx/dz=10$
- $dT/dt=6$

=0.6



=0.7



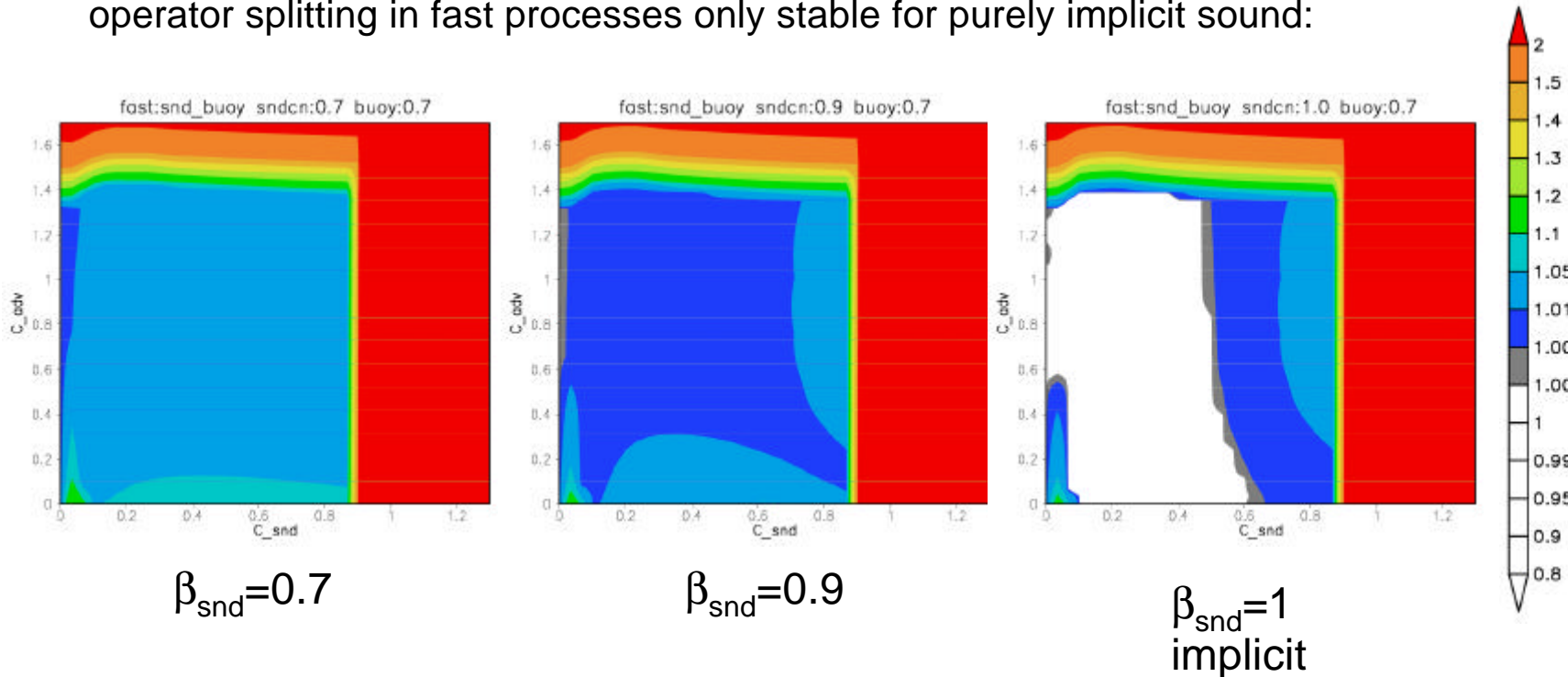
'Sound -> Div. -> Buoyancy'

'(Sound+Buoyancy) -> Div.'

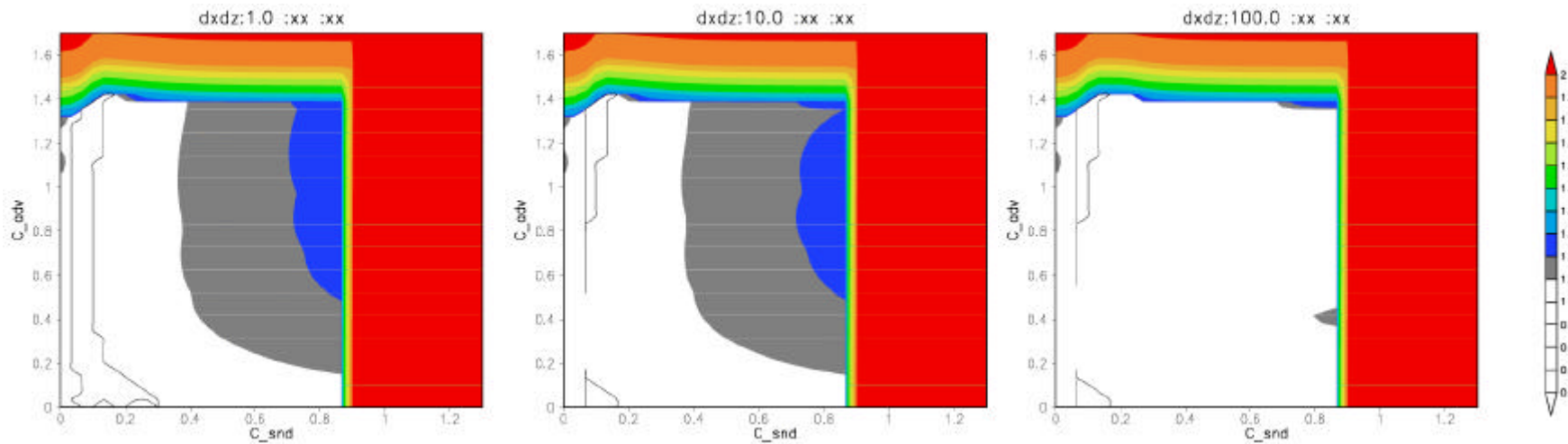
'Sound+Div.+Buoyancy'

curious result:
operator splitting of all the fast processes is not the best choice,
better: simple addition of tendencies.

operator splitting in fast processes only stable for purely implicit sound:



What is the influence of the grid anisotropy?



$\Delta x:\Delta z=1$

$\Delta x:\Delta z=10$

$\Delta x:\Delta z=100$

Conclusions from stability analysis of the 2-timelevel splitting schemes

- KW-RK2 allows only smaller time steps with upwind 5. order than RK3 → RK3 is more accurate and more efficient (!) than RK2
- Divergence filtering is needed ($C_{\text{div},x} = 0.1$: good choice) to stabilize purely horizontal waves.
Even KW-Euler-Forward-scheme can be stabilized by a (strong) divergence damping (stability analysis by Skamarock, Klemp (1992) too carefully)
- bigger $\Delta x/\Delta z$ seems not to be problematic for stability
- increasing $\Delta T/\Delta t$ does not reduce stability
prove for no stability constraint for n_s in the 1D sound-advection-system
- buoyancy in fast processes: better addition of tendencies than operator splitting (operator splitting needs purely implicit scheme for the sound)
in case of stability problems: reduction of small time step recommended

Test of the dynamical core: linear, hydrostatic mountain wave

$dx=2000\text{m}$, $N=0.018\text{ 1/s}$, $t=30\text{h}$

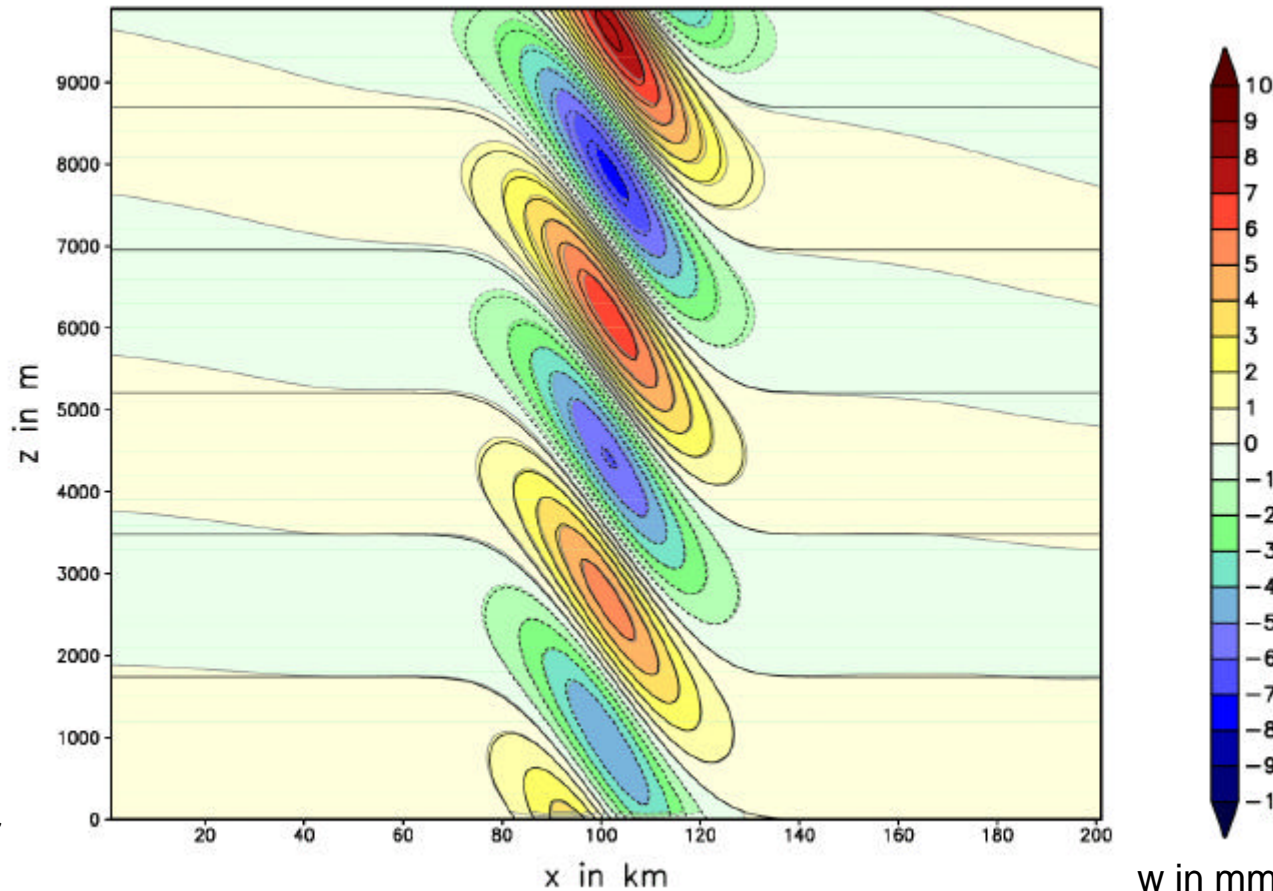
Gaussian hill
Half width = 40 km
Height = 10 m
 $U_0 = 10\text{ m/s}$
isothermal stratification

$dx=2\text{ km}$
 $dz=100\text{ m}$
 $T=30\text{ h}$

analytic solution:
black lines

simulation:
colours + grey lines

RK 3. order + upwind 5. order



Question: can time splitting schemes deliver a correct stationary solution?

Example: **scalar relaxation equation with external force** (Murthy, Nanjundiah, 2000)

$$\frac{d\phi}{dt} = \underbrace{-\beta\phi}_{\text{Relax.}} + \underbrace{g}_{\text{Force}}, \quad \beta > 0, \beta, g \text{ constant}$$

stationary solution:

$$\phi_s = \frac{g}{\beta}$$

Discretisation of single processes with simple Euler-forward-schemes; resulting stationary solution of the numerical time splitting system:

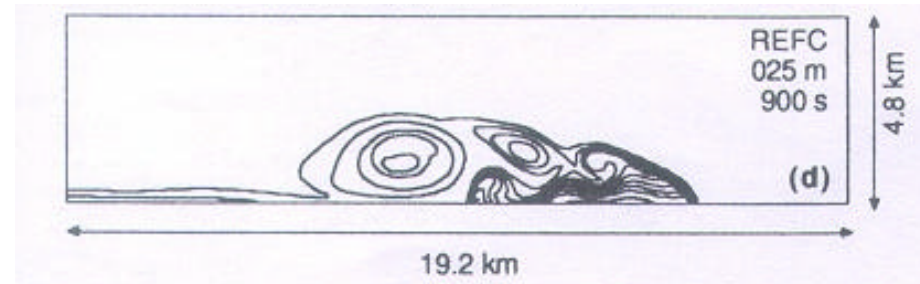
Splitting	Relax. fast, Forcing slow	Forcing fast, Relax. slow
Additive	$g/\beta \cdot \left(1 + \frac{1}{2} \frac{n_s-1}{n_s} \beta \Delta t + \dots\right)$	$g/\beta \cdot (1 - \beta \Delta T)$
KW-EV	g/β	g/β
KW-Leapfrog	g/β	g/β
KW-RK2	g/β	g/β
KW-RK2-short	g/β	$g/\beta \cdot \left(1 - \beta \frac{\Delta T}{2}\right)$
KW-'RK3'	g/β	g/β
KW-RK3b	g/β	g/β

consistent solutions for $\Delta T, \Delta t \rightarrow 0$, but in practice: $\beta \Delta T \approx 1$ or $\beta \Delta t \approx 1$

(Baldauf, 2004)

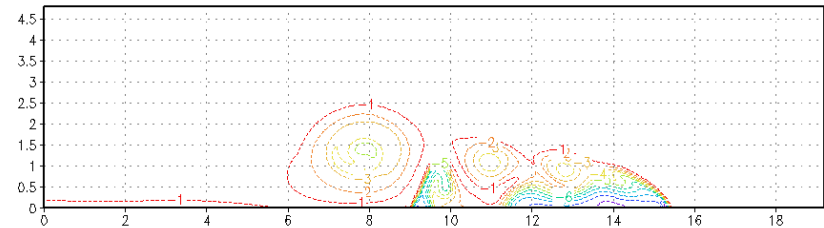
Test of the dynamical core: density current (Straka et al., 1993)

θ' after 900 s. (Reference)
by Straka et al. (1993)



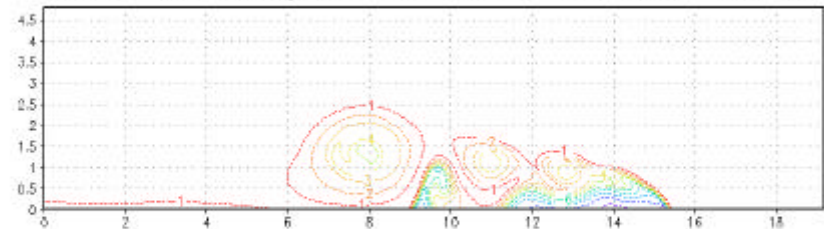
RK3 + upwind 5. order

Straka-Test thetap d = 50 m t = 15 min : 00 sec



RK2 + upwind 3. order

Straka-Test thetap d = 50 m t = 15 min : 00 sec



Implicit Vertical Advection for dynamic variables (u, v, w, T, p')

$$\frac{\partial f}{\partial t} + c \frac{\partial f}{\partial z} = M$$

Generalized Crank-Nicholson-advection

$$\frac{f_j^{n+1} - f_j^n}{\Delta t} + \frac{c_j}{\Delta z} \cdot \left(\underbrace{\beta A_j^{n+1}}_{\text{implicit}} + \underbrace{(1 - \beta) A_j^n}_{\text{explicit}} \right) = M_j^n \quad C_j = c_j \frac{\Delta t}{\Delta z}$$

(Dimensionless) Advection operator for centered differences 2. order (3-point-stencil):

$$A_j^n = \frac{1}{2} f_{j+1}^n - \frac{1}{2} f_{j-1}^n$$

- Ⓜ Lin. eq. system with a tridiagonal matrix, needs $\sim 3 N$ operations

Motivation for a better scheme:
explicitly resolved convection, higher values of w

dim.less advection operator for upwind 3. order (4-point stencil)

$$A_j^n := \left(\frac{1}{6} + \frac{C_j^2}{12} \right) f_{j-2}^n + \left(-1 - \frac{C_j^2}{4} \right) f_{j-1}^n + \left(\frac{1}{2} + \frac{C_j^2}{4} \right) f_j^n + \left(\frac{1}{3} - \frac{C_j^2}{12} \right) f_{j+1}^n$$

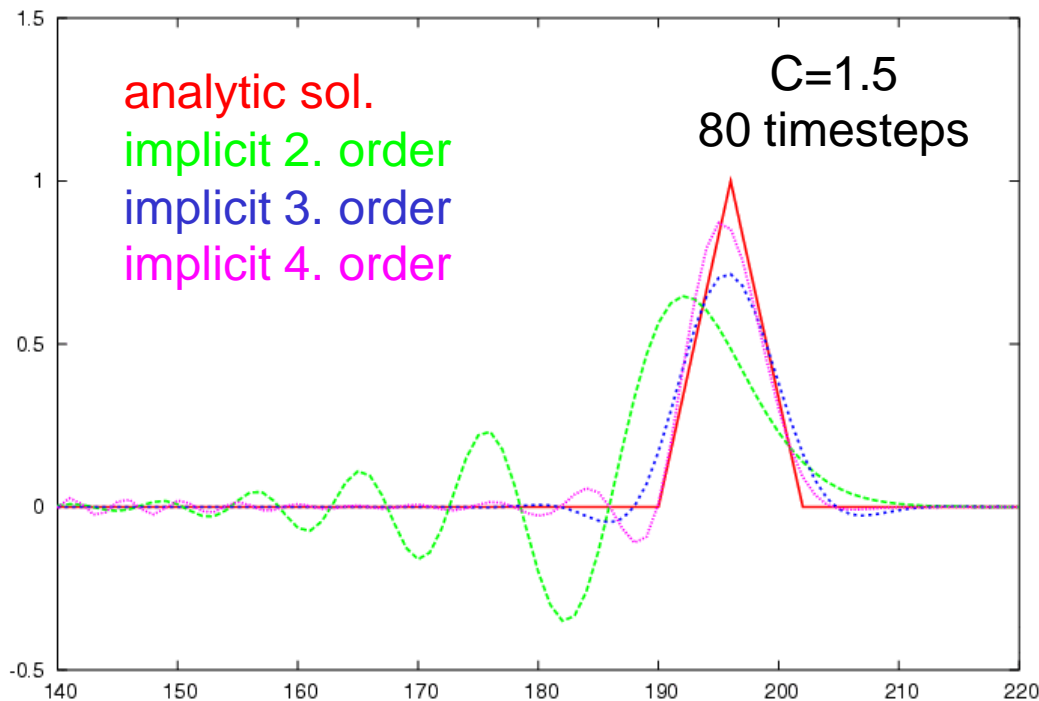
case $C_j > 0$

(¹ Crowley 3. order, e.g. Tremback et al., 1987)

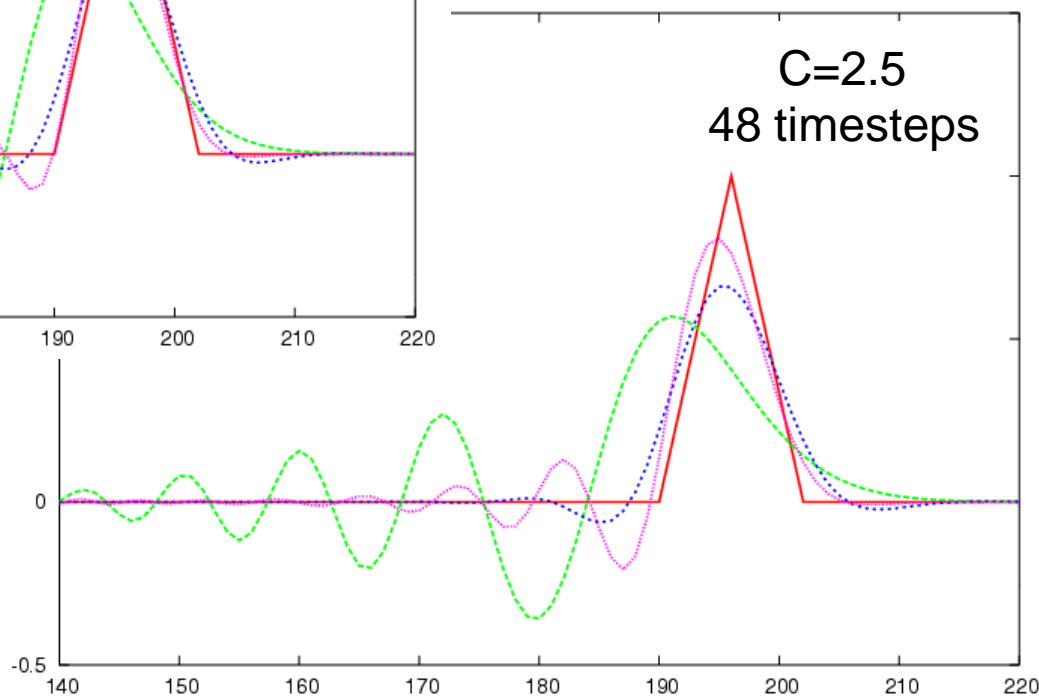
- $\beta = 1/2$: unconditionally stable, damping, truncation error 3. order
- $\beta > 1/2$: unconditionally stable, damping, trunc. error 1. order
- $\beta < 1/2$: unstable

Lin. eq. system with a 5-band diagonal matrix
needs $\sim 14 N$ operations

LMK: Subr. ‚complete_tendencies_uvwTpp_CN3‘



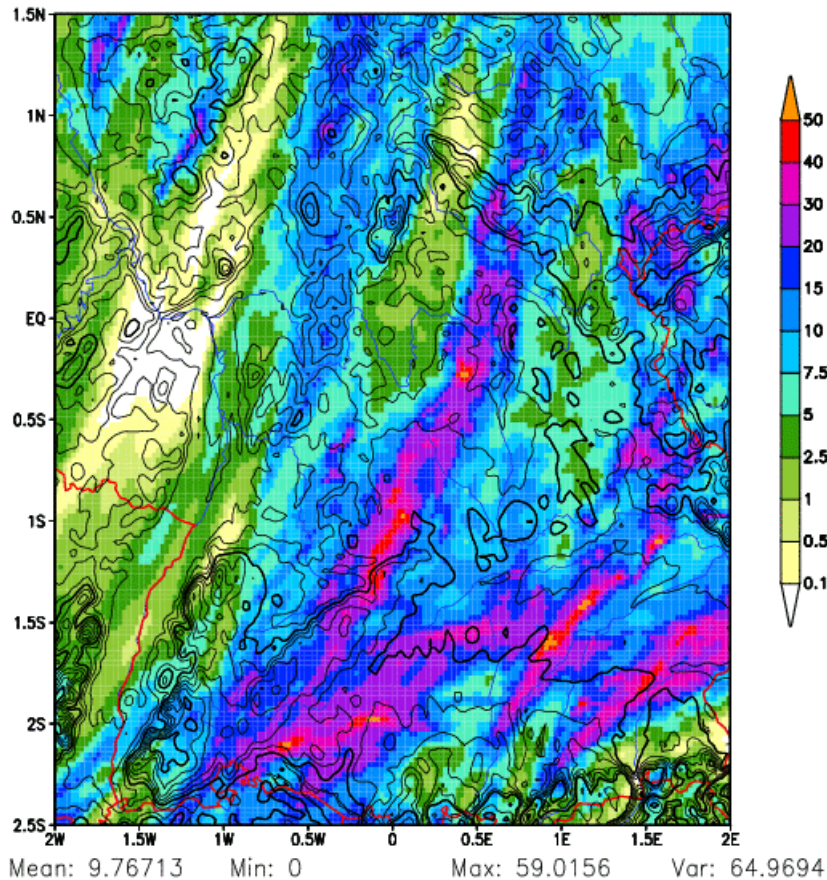
Idealized 1D advection test



Real case study: LMK (2.8 km resolution) ,12.08.2004, 12UTC-run'

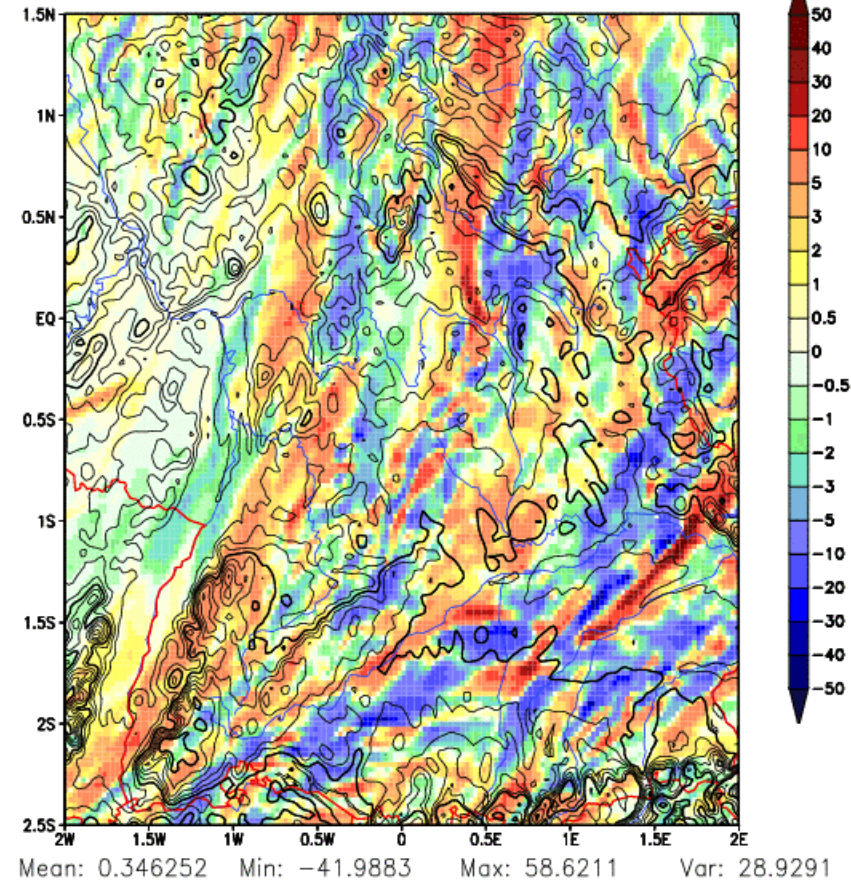
implicit vertical adv. 2. order

12.08.2004,12UTC+1800h, totprec, 1D



difference: 3. order - 2. order

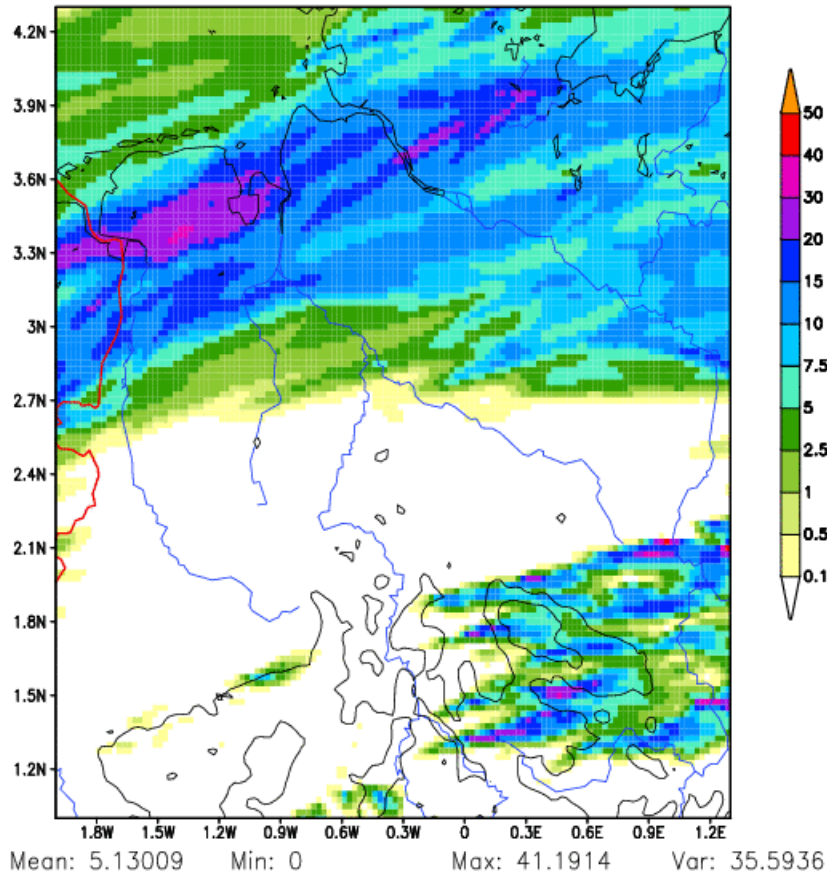
12.08.2004,12 UTC, 1800-1800 h, totprec: CN3-CN2



Real case study: LMK (2.8 km resolution), 25.06.2005, 00UTC-run'

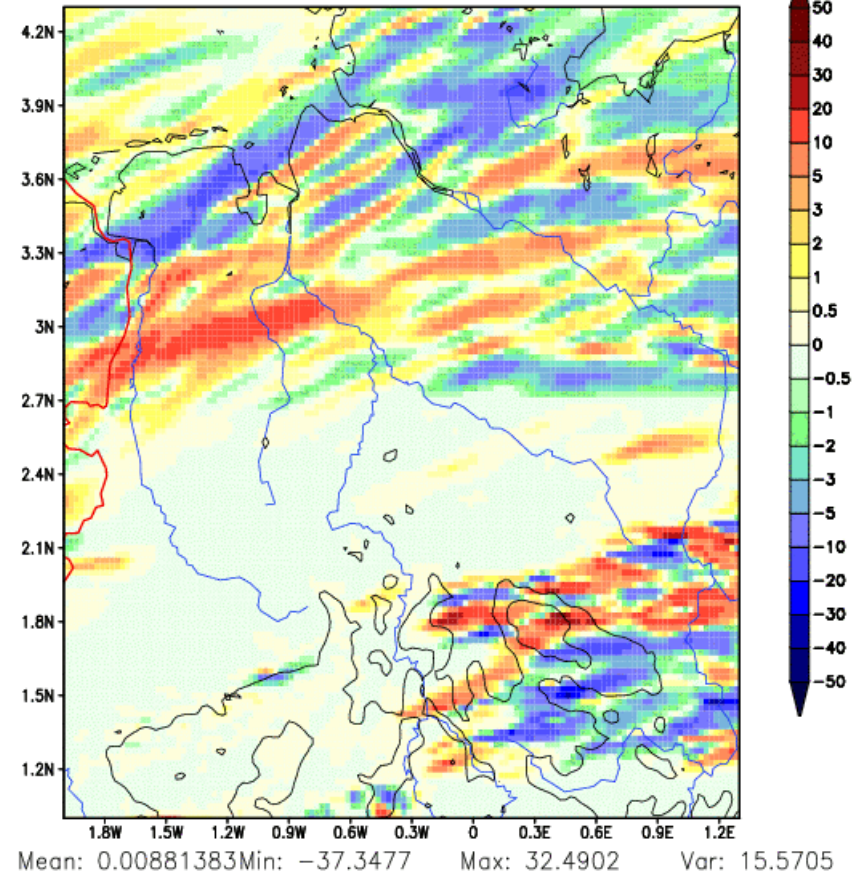
implicit vertical adv. 2. order

25.06.2005,00UTC+1800h, totprec, 1D



difference: 3. order - 2. order

25.06.2005,00 UTC, 1800-1800 h, totprec: CN3-CN2



2-dim. horizontal Advection

- 2D-advection in RK-schemes by a simple adding of tendencies (operator splitting (e.g. corner transport upstream (CTU) method) is not possible for upstream 3., 5., ... order)
- this is limited by

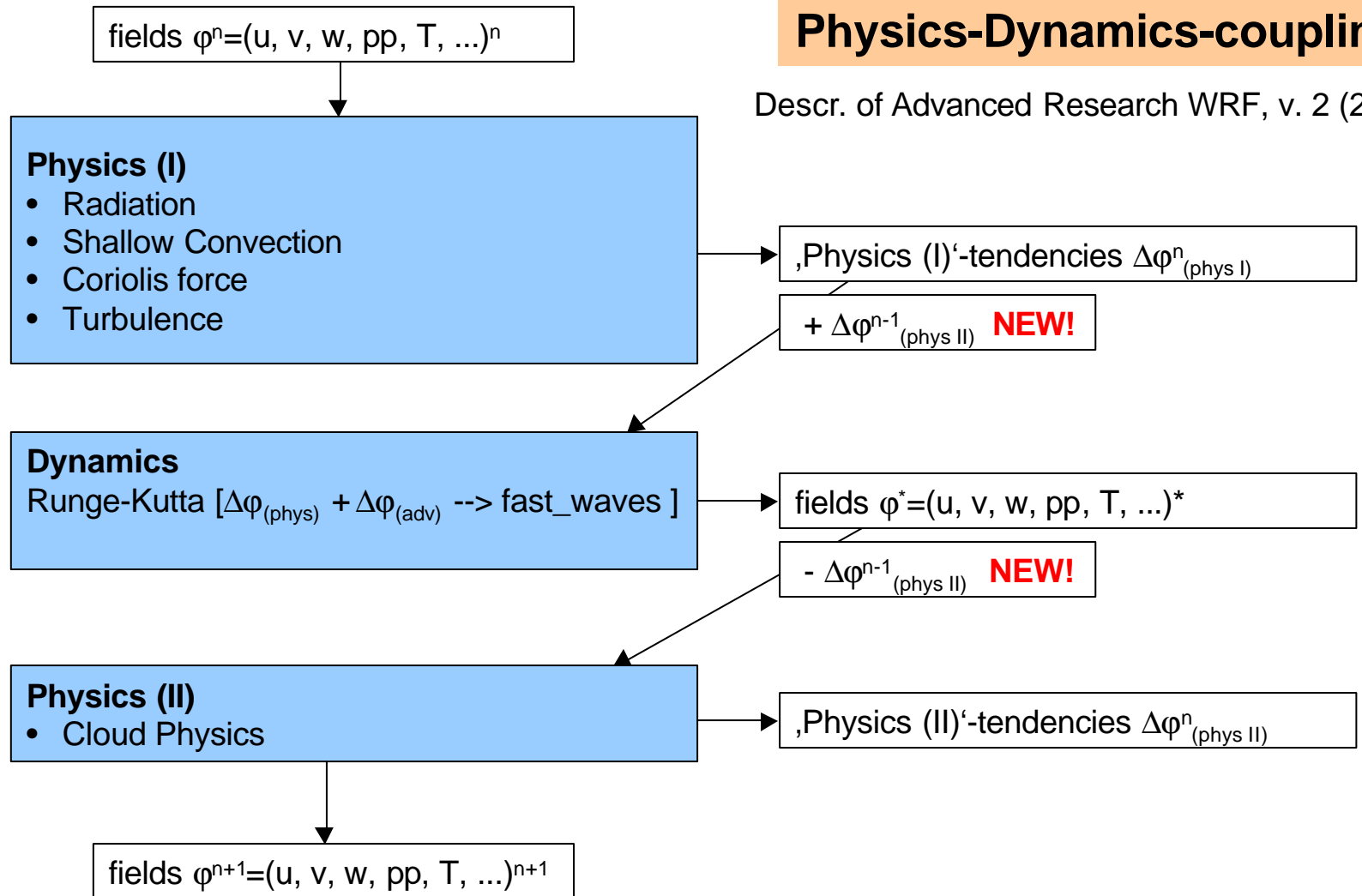
$$|C_x| + |C_y| < \text{const.}$$

can be proven for RK2 + upwind 3. order

it holds empirically also for RK3 + upwind 5. order

- compare with the usual formulated 2-dimensional stability criterion:

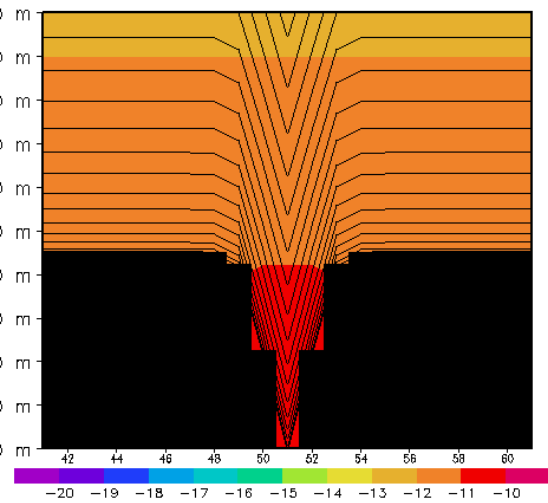
$$\Delta t < \frac{\Delta s}{\sqrt{2} |\mathbf{v}|} \Rightarrow |\mathbf{C}| < \frac{1}{\sqrt{2}}$$



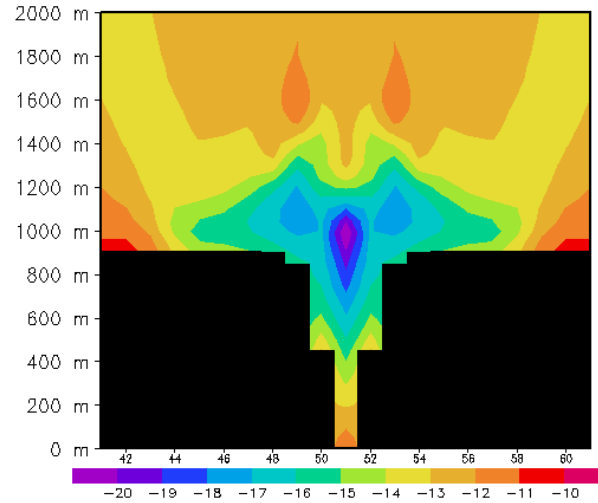
Physics-Dynamics-coupling

Descr. of Advanced Research WRF, v. 2 (2005)

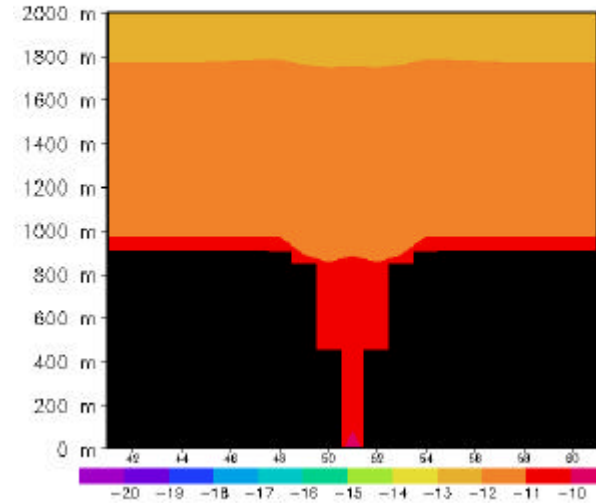
cold pool – problem in narrow valleys
is essentially induced by pressure gradient term



starting point T (°C)



after 1 h



after 1 h

modified version:

pressure gradient on z-levels, if
 $|\text{metric term}| > |\text{terrain follow. te}$

Numerical questions currently considered:

- Properties of time-splitting (Runge-Kutta) schemes:
 - convergence (in linear/nonlinear cases, dynamical core alone/with physics, ...)
 - accuracy
 - conservation
- Implicit vertical advection for dynamic variables
- fast-waves-solver (strong conservation form, ...)
- upper radiative boundary condition
- Physics-Dynamics coupling
 - originally changed due to an underestimation of precipitation in convective events because of too weak coupling
 - problems in turbulence scheme (?)
 - Bryan, Fritsch (2002) test case
- (terrain-following coordinate in steep terrain)
Cold pools in narrow, deep valleys



ENDE

Time-splitted Euler forward step

