

Status of RADVOP – Efficient radar forward operator for data assimilation and model verification

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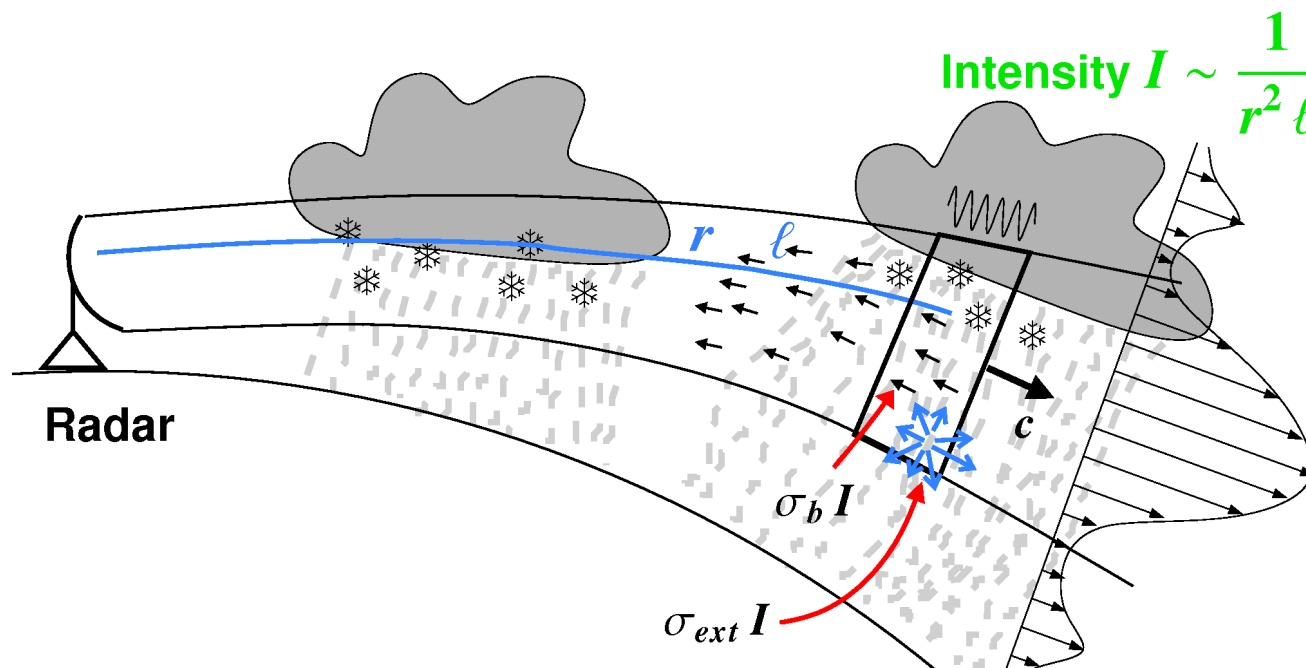
³MeteoSwiss

COSMO General Meeting, Rome, 05.09.2011

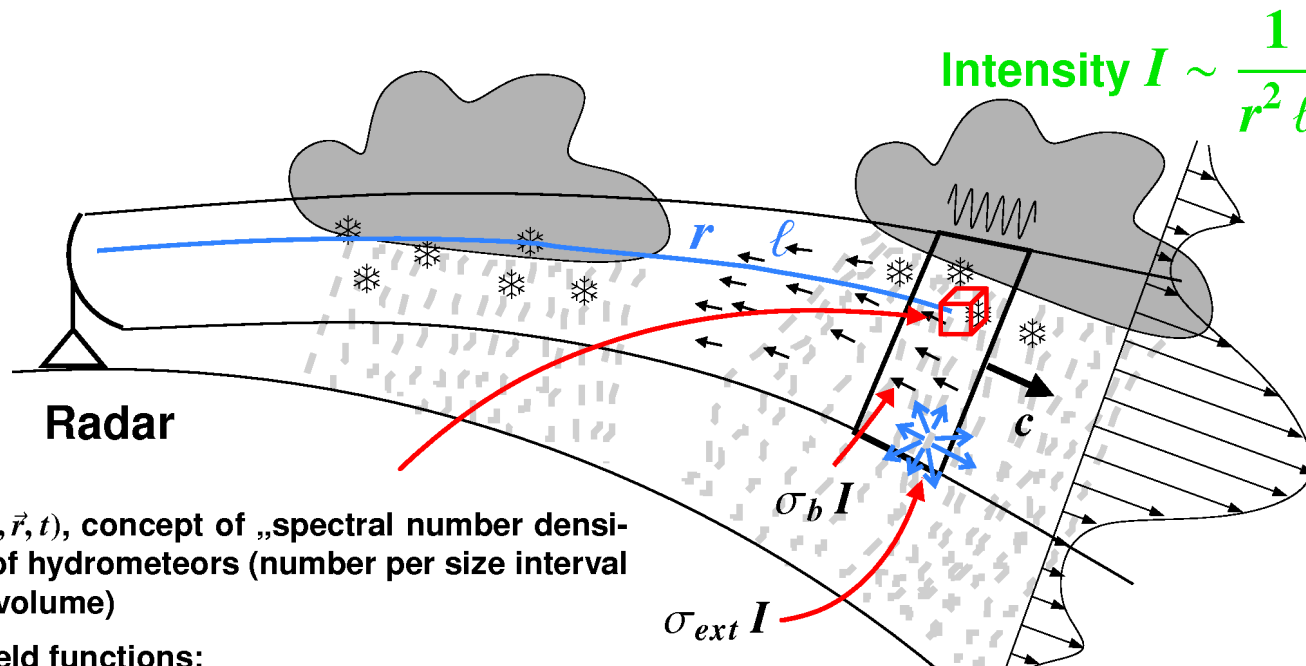
- Possible enhancement of the short-range precipitation forecast by
 - a) assimilation of radar data
 - b) microphysics enhance-ments derived from comparisons of model results with radar data
- DWD:

Up to now: latent heat nudging and simple nudging of radial winds.
Future: ENTKF assimilation system based on COSMO-DE-EPS.
For assimilation of radar data socalled „forward operator“ necessary (simulation of radar quantities on the basis of model results on the native radar grid: **radial winds, reflektivty, polarisation parameters**).
- Such a forward operator also helpful for comparisons of model results and radar directly in terms of radar measurables - much easier than instead trying to derive model quantities like 3D wind, precipitation and hydrometeor contents from radar data.
- Project within the Extramural Research Program.
- Requirement: **parallel / vectorized operator, integrated in COSMO code**

Principle of radar measurement



Principle of radar measurement



$N(D, \vec{r}, t)$, concept of „spectral number density“ of hydrometeors (number per size interval per volume)

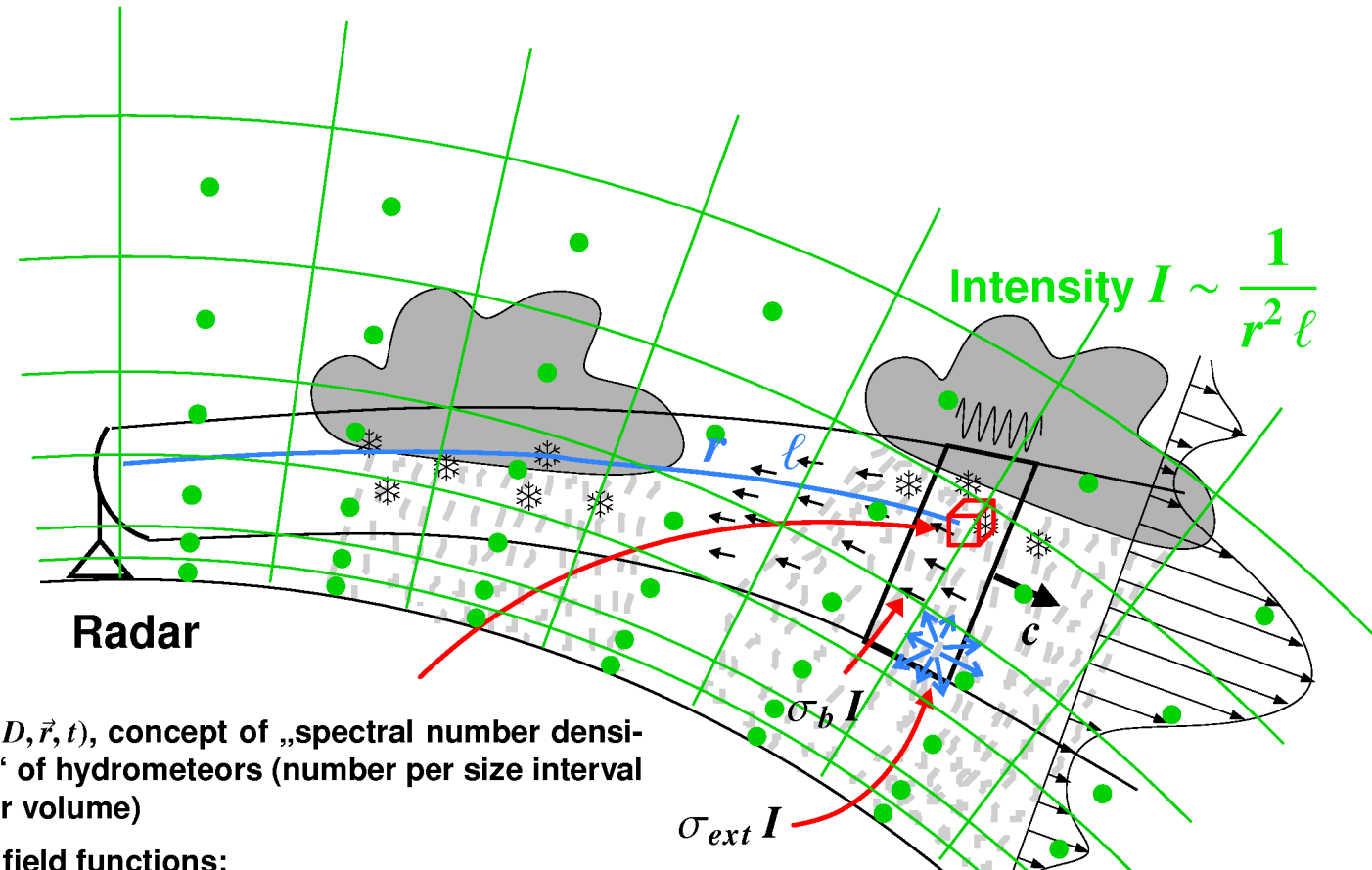
⇒ field functions:

$$\eta = \int_0^{\infty} \sigma_b(D) N(D) dD \quad \Lambda = \int_0^{\infty} \sigma_{ext}(D) N(D) dD$$

~ Z_e

useful for atten. (assumption: incoherent single scattering)

Principle of radar measurement



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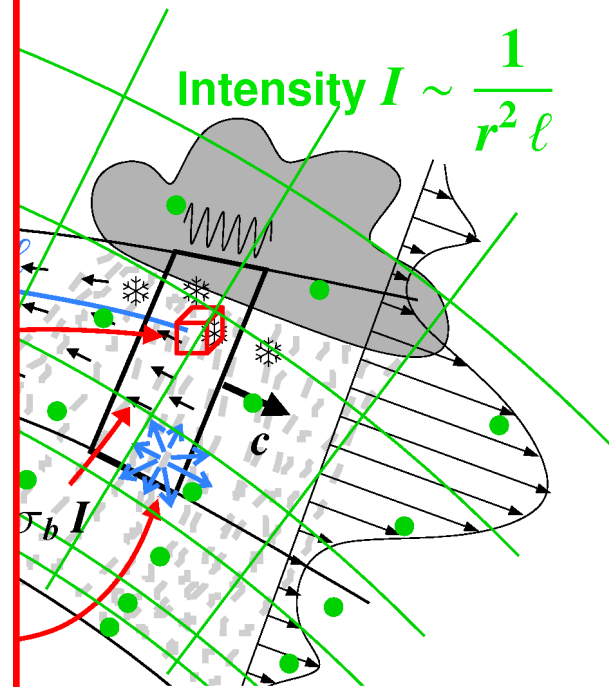
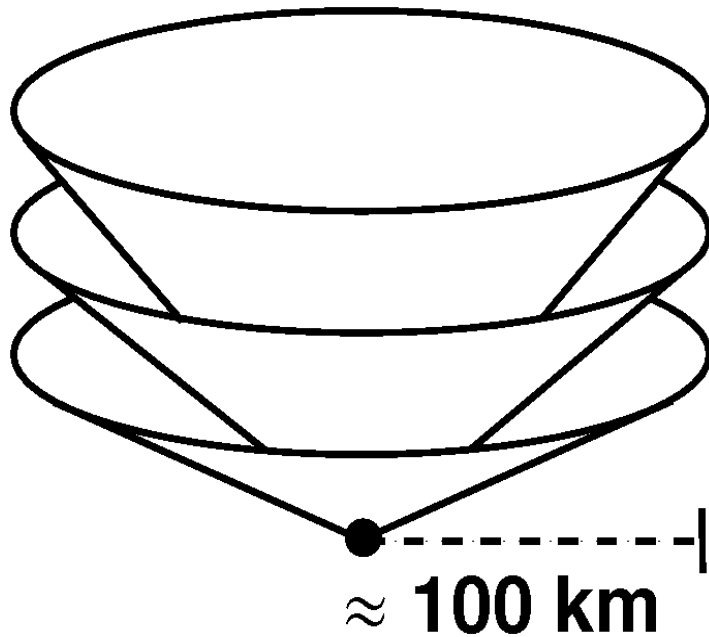
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Principle of radar measurement

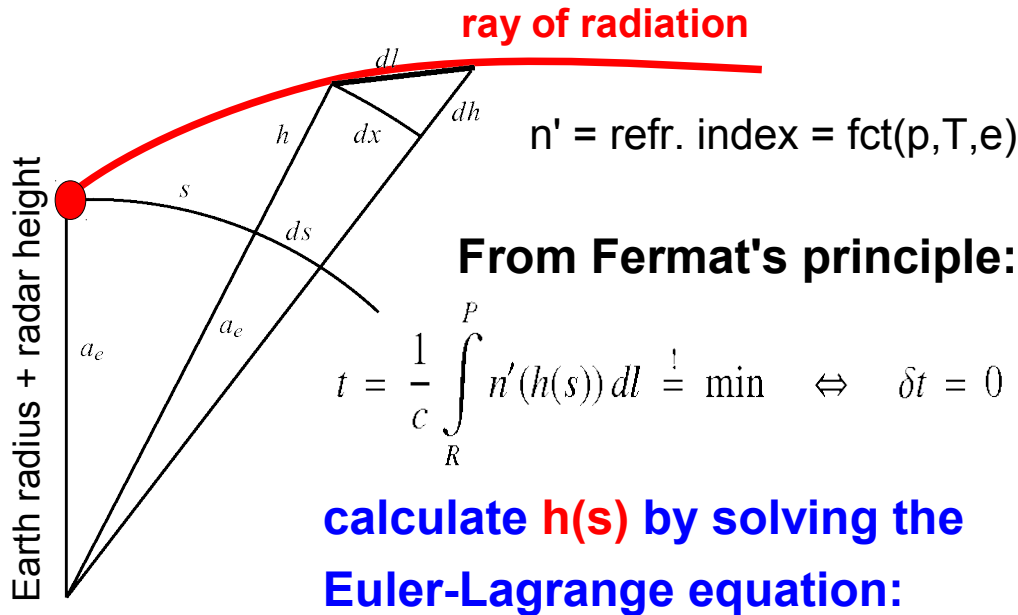
Meßzeit ≈ 10 min



$\sim Z_e$

useful for atten. (assumption: incoherent single scattering)

Atmospheric ray propagation



$$t = \frac{1}{c} \int_R^P n'(h(s)) dl \stackrel{!}{=} \min \Leftrightarrow \delta t = 0$$

calculate $h(s)$ by solving the Euler-Lagrange equation:

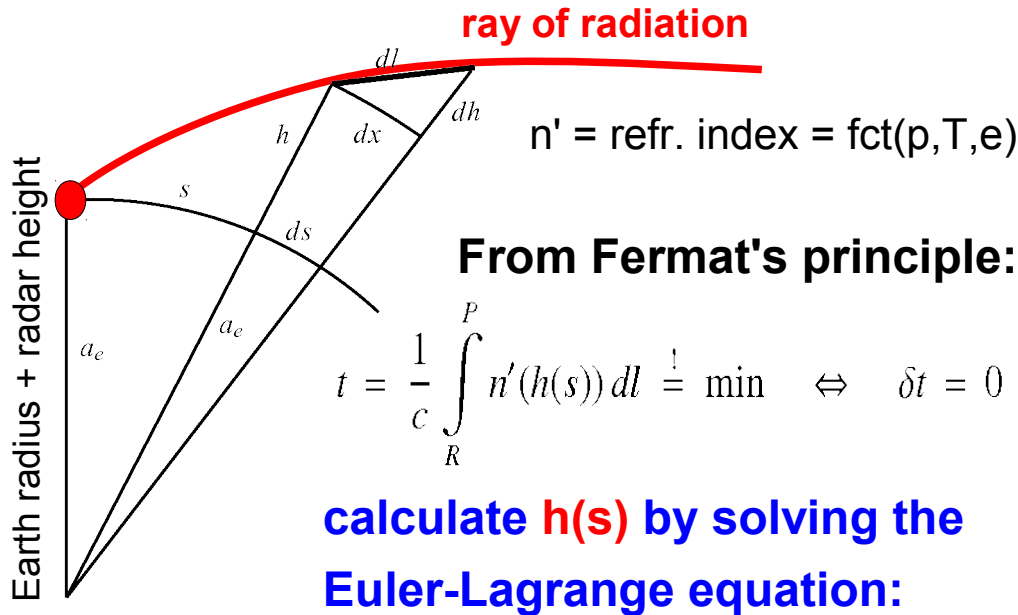
$$\frac{d^2 h}{ds^2} - \left(\frac{1}{n'} \frac{dn'}{dh} + \frac{2}{a_e + h} \right) \left(\frac{dh}{ds} \right)^2 - \left(\frac{a_e + h}{a_e} \right)^2 \left(\frac{1}{n'} \frac{dn'}{dh} + \frac{1}{a_e + h} \right) = 0$$

or by making use of its conserved integral:

$$n' (h + a_e) \cos(\epsilon_{loc}) = \text{const.}$$

where $\epsilon_{loc} = \arctan \left(\frac{dh}{dx} \right) = \arctan \left(\frac{a_e}{a_e + h} \frac{dh}{ds} \right)$

Atmospheric ray propagation



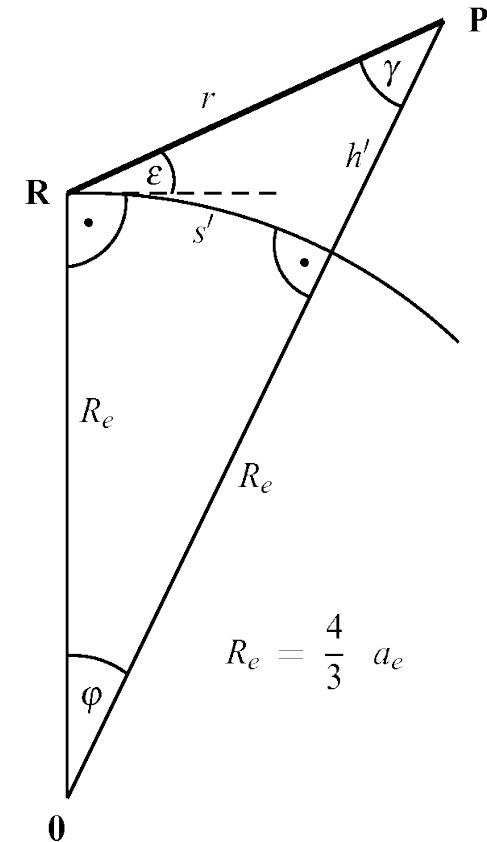
$$\frac{d^2 h}{ds^2} - \left(\frac{1}{n'} \frac{dn'}{dh} + \frac{2}{a_e + h} \right) \left(\frac{dh}{ds} \right)^2 - \left(\frac{a_e + h}{a_e} \right)^2 \left(\frac{1}{n'} \frac{dn'}{dh} + \frac{1}{a_e + h} \right) = 0$$

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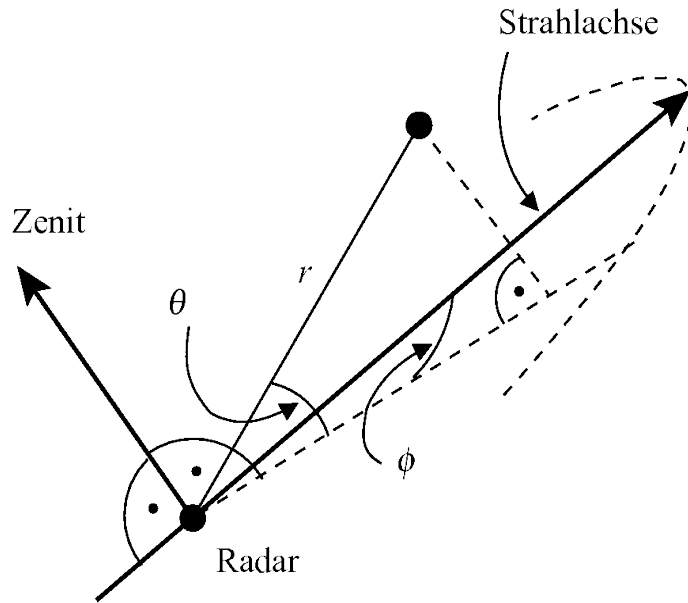
$$n' (h + a_e) \cos(\epsilon_{loc}) = \text{const.}$$

where $\epsilon_{loc} = \arctan \left(\frac{dh}{dx} \right) = \arctan \left(\frac{a_e}{a_e + h} \frac{dh}{ds} \right)$

Efficient approximation for „standard“ conditions:
4/3 – earth - model



Radar operator (reflectivity)



$$f^2(\phi, \theta) = \exp\left(-4 \ln 2 \left(\frac{\phi^2}{\phi_3^2} + \frac{\theta^2}{\theta_3^2}\right)\right)$$

$$\eta(r, \phi, \theta) = \int_0^{\infty} \sigma_b(D) N(D, r, \phi, \theta) dD$$

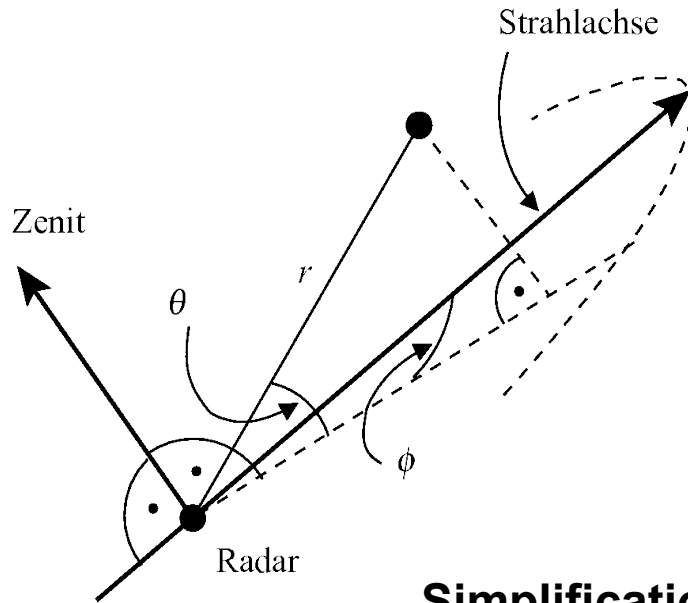
$$Z_e = \eta \frac{\lambda_0^4}{\pi^5 |K_w|^2}$$

$$\langle Z_e^{(R)} \rangle = \frac{\int_{r_0 - \Delta r/2}^{r_0 + \Delta r/2} \int_{-\pi}^{\pi} \int_{-\pi/2}^{\pi/2} Z_e(r, \phi, \theta) \exp\left[-2 \int_0^r \int_0^{\infty} \sigma_{ext}(D) N(D, r', \phi, \theta) dD dr'\right] \frac{f(\phi, \theta)^4}{r^2} \cos \theta d\theta d\phi dr}{\int_{r_0 - \Delta r/2}^{r_0 + \Delta r/2} \int_{-\pi}^{\pi} \int_{-\pi/2}^{\pi/2} \frac{f(\phi, \theta)^4}{r^2} \cos \theta d\theta d\phi dr}$$

$L_N^{-2}(r, \phi, \theta)$

$\Lambda(r', \phi, \theta)$

Radar operator (reflectivity)



$$f^2(\phi, \theta) = \exp\left(-4 \ln 2 \left(\frac{\phi^2}{\phi_3^2} + \frac{\theta^2}{\theta_3^2}\right)\right)$$

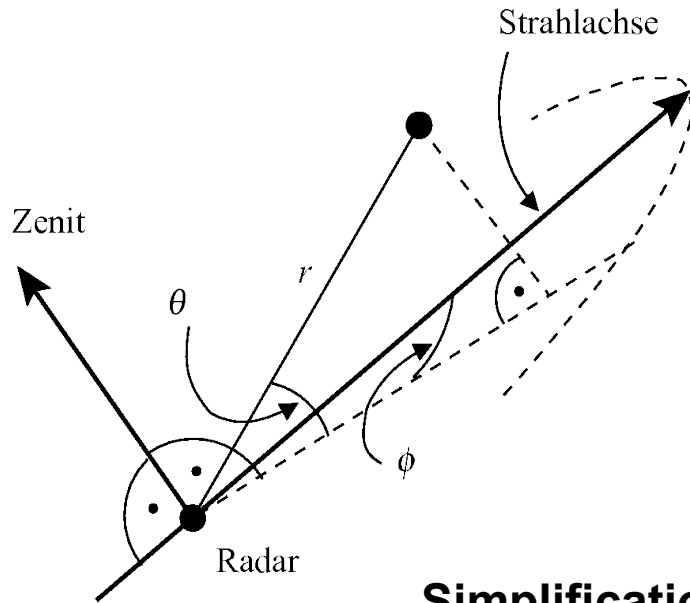
$$\eta(r, \phi, \theta) = \int_0^{\infty} \sigma_b(D) N(D, r, \phi, \theta) dD$$

$$Z_e = \eta \frac{\lambda_0^4}{\pi^5 |K_w|^2}$$

Simplification 1:

$$\langle Z_e^{(R)} \rangle = \frac{\int_{\pi/2}^{\pi/2} Z_e(r_0, 0, \theta) \exp\left[-2 \int_0^{r_0} \int_0^{\infty} \sigma_{ext}(D) N(D, r', \theta) dD dr'\right] f(0, \theta)^4 d\theta}{\int_{-\pi/2}^{\pi/2} f(0, \theta)^4 d\theta} \overbrace{I_N^{-2}(r_0, 0, \theta)}$$

Radar operator (reflectivity)



$$f^2(\phi, \theta) = \exp\left(-4 \ln 2 \left(\frac{\phi^2}{\phi_3^2} + \frac{\theta^2}{\theta_3^2}\right)\right)$$

$$\eta(r, \phi, \theta) = \int_0^{\infty} \sigma_b(D) N(D, r, \phi, \theta) dD$$

$$Z_e = \eta \frac{\lambda_0^4}{\pi^5 |K_w|^2} \quad k_2 = \frac{20}{\ln 10} \Lambda$$

Simplification 2:

$$\langle Z_e^{(R)} \rangle = Z_e(r_0, 0, 0) \exp\left(-2 \int_0^{r_0} \int_0^{\infty} \sigma_{ext}(D) N(D, r') dD dr'\right) \overbrace{\quad}^{I_N^{-2}(r_0, 0, 0)}$$

Approximations for Z_e

In general: Mie-scattering (one- or two-layered spheres) :

$$\sigma_{\text{back}} = f(D, m) \quad , \quad m = \text{refract. index hydrometeors} \\ (\text{ice/water/air-mixtures})$$

$$\sigma_{\text{ext}} = f(D, m)$$

Approximations:

Rayleigh: $\sigma_{\text{back}} \sim D^6$

→ **water drops:** $Z_e \sim M_6$ (analytic for gamma size distr.)

→ **ice hydrom.:** m variable, still need to integrate over $N(D)$

→ **small dry ice hydrom.:** Rayleigh + Debye-approx. for m :

$$Z_e \sim \rho_{\text{snow}}^2(D) M_6$$

Radial wind operator and simplif.

$$\langle v_r^{(R)} \rangle = \frac{\int_{r_0-\Delta r/2}^{r_0+\Delta r/2} \int_{-\pi}^{\pi} \int_{-\pi/2}^{\pi/2} (\vec{v} \cdot \vec{e}_r) \frac{\eta}{l_n^2} \frac{f^4}{r^2} \cos(\theta) d\theta d\phi dr}{\int_{r_0-\Delta r/2}^{r_0+\Delta r/2} \int_{-\pi}^{\pi} \int_{-\pi/2}^{\pi/2} \frac{\eta}{l_n^2} \frac{f^4}{r^2} \cos(\theta) d\theta d\phi dr} - \frac{\int_{r_0-\Delta r/2}^{r_0+\Delta r/2} \int_{-\pi}^{\pi} \int_{-\pi/2}^{\pi/2} (\vec{e}_3 \cdot \vec{e}_r) \bar{v}_T \frac{\eta}{l_n^2} \frac{f^4}{r^2} \cos(\theta) d\theta d\phi dr}{\int_{r_0-\Delta r/2}^{r_0+\Delta r/2} \int_{-\pi}^{\pi} \int_{-\pi/2}^{\pi/2} \frac{\eta}{l_n^2} \frac{f^4}{r^2} \cos(\theta) d\theta d\phi dr}$$

With:

$$\bar{v}_T = \frac{\int_0^{\infty} \sigma_b(D) N(D) v_T(D) dD}{\eta}$$

$$l_n^{-2} = \exp \left(-2 \int_0^r \Lambda(r') dr' \right)$$

Refl.-weighted hydrom. fall speed
(computed from model variables or
somehow approximated)

Attenuation factor

Radial wind operator and simplif.

$$\langle v_r^{(R)} \rangle = \frac{\int_{r_0-\Delta r/2}^{r_0+\Delta r/2} \int_{-\pi}^{\pi} \int_{-\pi/2}^{\pi/2} (\vec{v} \cdot \vec{e}_r) \frac{\eta}{l_n^2} \frac{f^4}{r^2} \cos(\theta) d\theta d\phi dr}{\int_{r_0-\Delta r/2}^{r_0+\Delta r/2} \int_{-\pi}^{\pi} \int_{-\pi/2}^{\pi/2} \frac{\eta}{l_n^2} \frac{f^4}{r^2} \cos(\theta) d\theta d\phi dr} - \frac{\int_{r_0-\Delta r/2}^{r_0+\Delta r/2} \int_{-\pi}^{\pi} \int_{-\pi/2}^{\pi/2} (\vec{e}_3 \cdot \vec{e}_r) \bar{v}_T \frac{\eta}{l_n^2} \frac{f^4}{r^2} \cos(\theta) d\theta d\phi dr}{\int_{r_0-\Delta r/2}^{r_0+\Delta r/2} \int_{-\pi}^{\pi} \int_{-\pi/2}^{\pi/2} \frac{\eta}{l_n^2} \frac{f^4}{r^2} \cos(\theta) d\theta d\phi dr}$$

Simplifications (examples):

Only vertical smoothing:

$$\langle v_r^{(R)} \rangle = \frac{\frac{\Delta r}{r_0^2} \int_{-\pi/2}^{\pi/2} (\vec{v} \cdot \vec{e}_r) \frac{\eta}{l_n^2} f^4(0, \theta) \cos(\theta) d\theta}{\frac{\Delta r}{r_0^2} \int_{-\pi/2}^{\pi/2} \frac{\eta}{l_n^2} f^4(0, \theta) \cos(\theta) d\theta} - \frac{\frac{\Delta r}{r_0^2} \int_{-\pi/2}^{\pi/2} (\vec{e}_3 \cdot \vec{e}_r) \bar{v}_T \frac{\eta}{l_n^2} f^4(0, \theta) \cos(\theta) d\theta}{\frac{\Delta r}{r_0^2} \int_{-\pi/2}^{\pi/2} \frac{\eta}{l_n^2} f^4(0, \theta) \cos(\theta) d\theta}$$

+ No reflectivity weighting.:

$$\langle v_r^{(R)} \rangle = \frac{\frac{\Delta r}{r_0^2} \int_{-\pi/2}^{\pi/2} (\vec{v} \cdot \vec{e}_r) f^4(0, \theta) \cos(\theta) d\theta}{\frac{\Delta r}{r_0^2} \int_{-\pi/2}^{\pi/2} f^4(0, \theta) \cos(\theta) d\theta} - \frac{\frac{\Delta r}{r_0^2} \int_{-\pi/2}^{\pi/2} (\vec{e}_3 \cdot \vec{e}_r) \bar{v}_T f^4(0, \theta) \cos(\theta) d\theta}{\frac{\Delta r}{r_0^2} \int_{-\pi/2}^{\pi/2} f^4(0, \theta) \cos(\theta) d\theta}$$

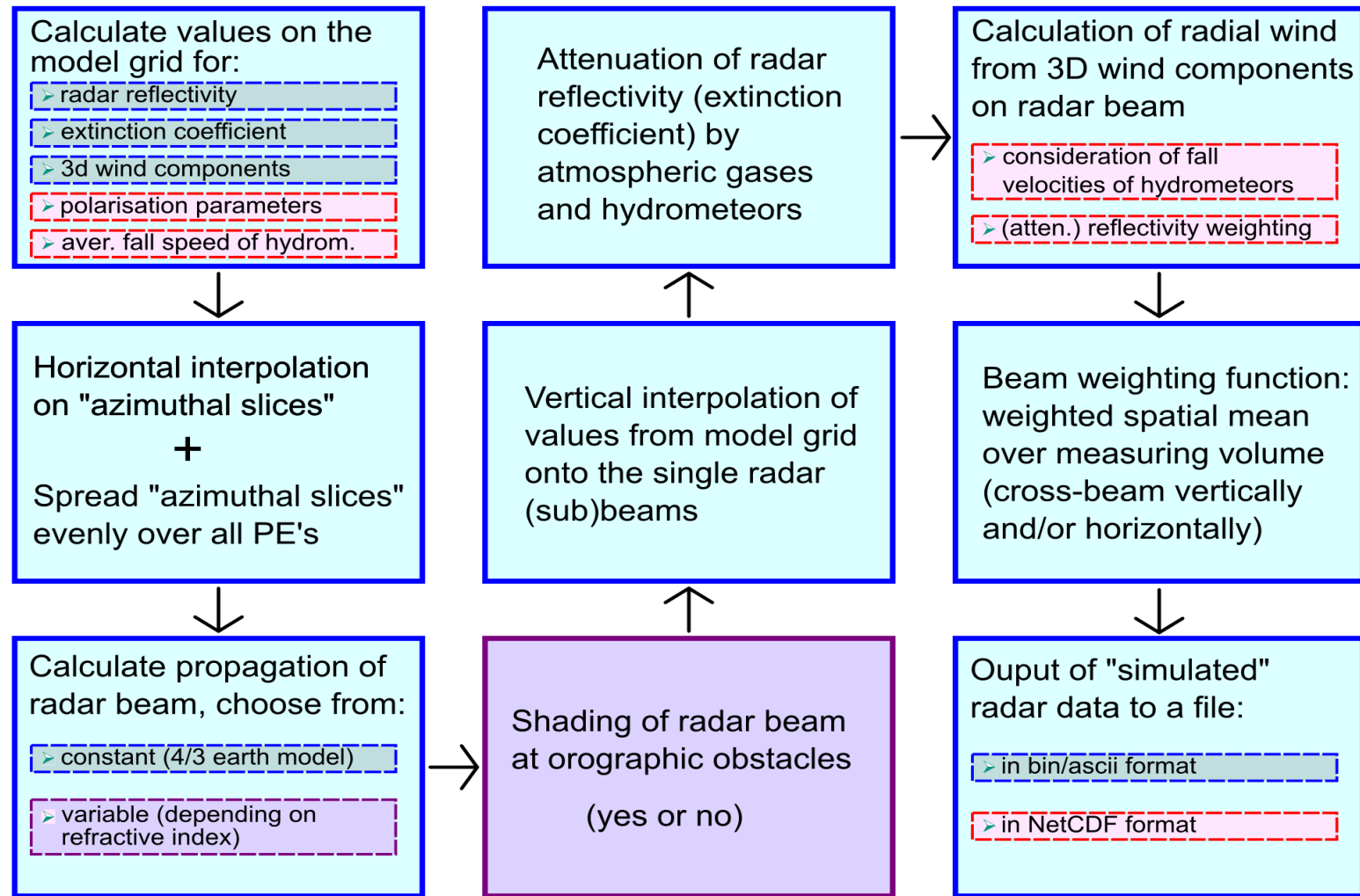
+ No hydrometeor fall speed:

$$\langle v_r^{(R)} \rangle = \frac{\frac{\Delta r}{r_0^2} \int_{-\pi/2}^{\pi/2} (\vec{v} \cdot \vec{e}_r) f^4(0, \theta) \cos(\theta) d\theta}{\frac{\Delta r}{r_0^2} \int_{-\pi/2}^{\pi/2} f^4(0, \theta) \cos(\theta) d\theta}$$

+ No smoothing, but with fall speed:

$$\langle v_r^{(R)} \rangle = \vec{v} \cdot \vec{e}_r + \bar{v}_T \vec{e}_3 \cdot \vec{e}_r$$

Block diagram and status

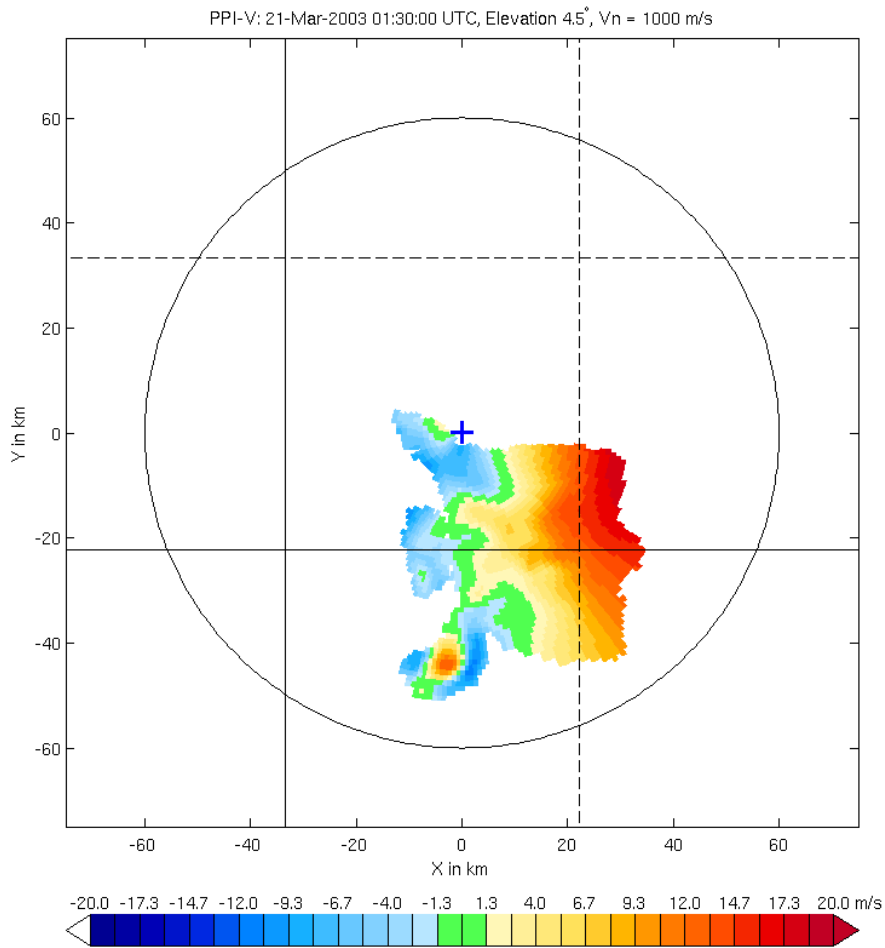


■ done / ready
 ■ in progress
 ■ to do

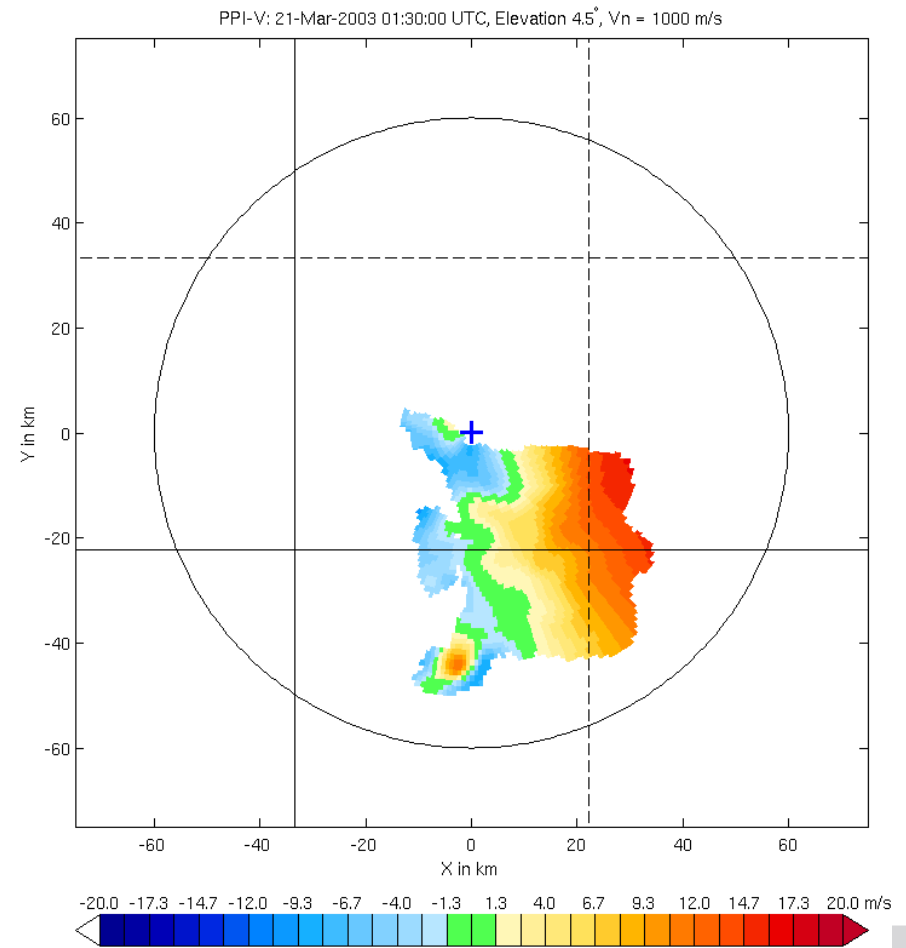
Results idealized convection 1 km

Radial wind

4/3 earth, no smoothing



4/3 earth, vertical smoothing

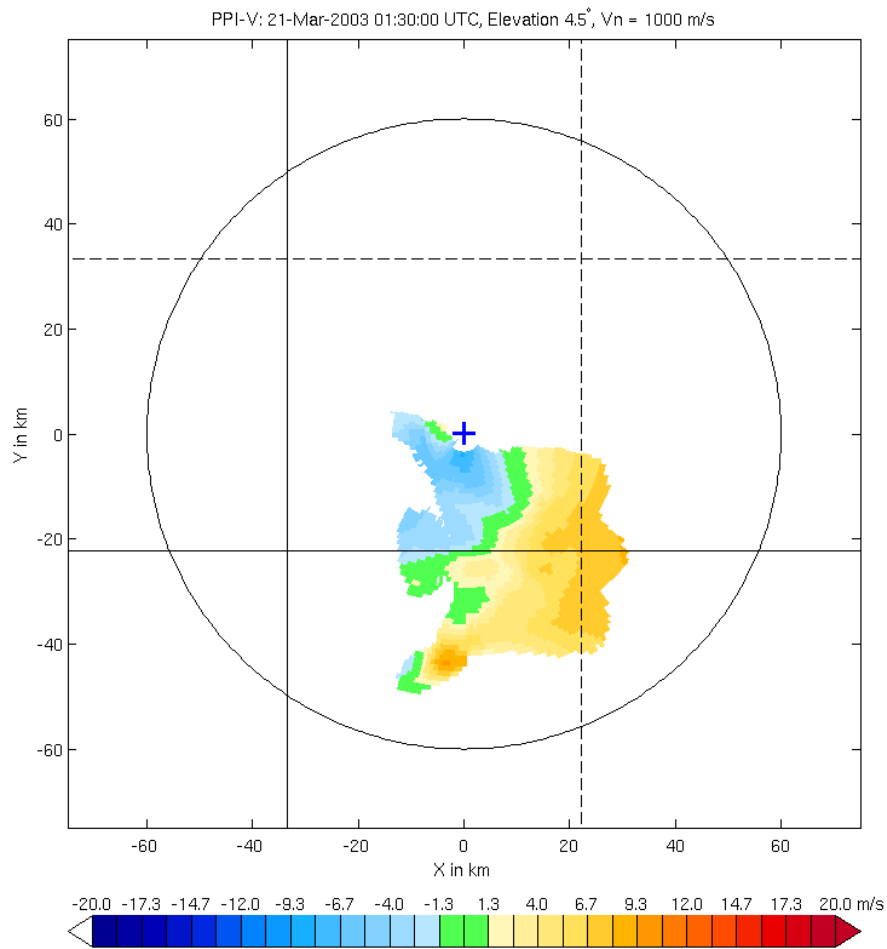


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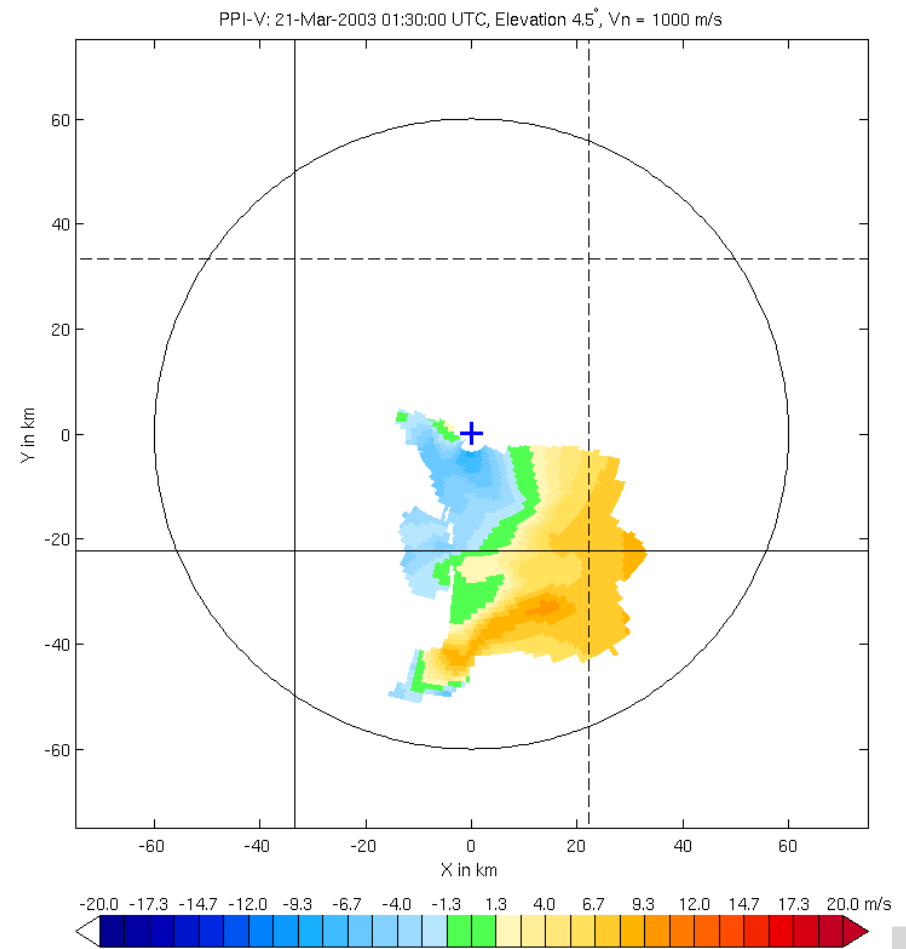
Results idealized convection 1 km

Radial wind

Online propag., no smoothing



Online propag., vertical smoothing



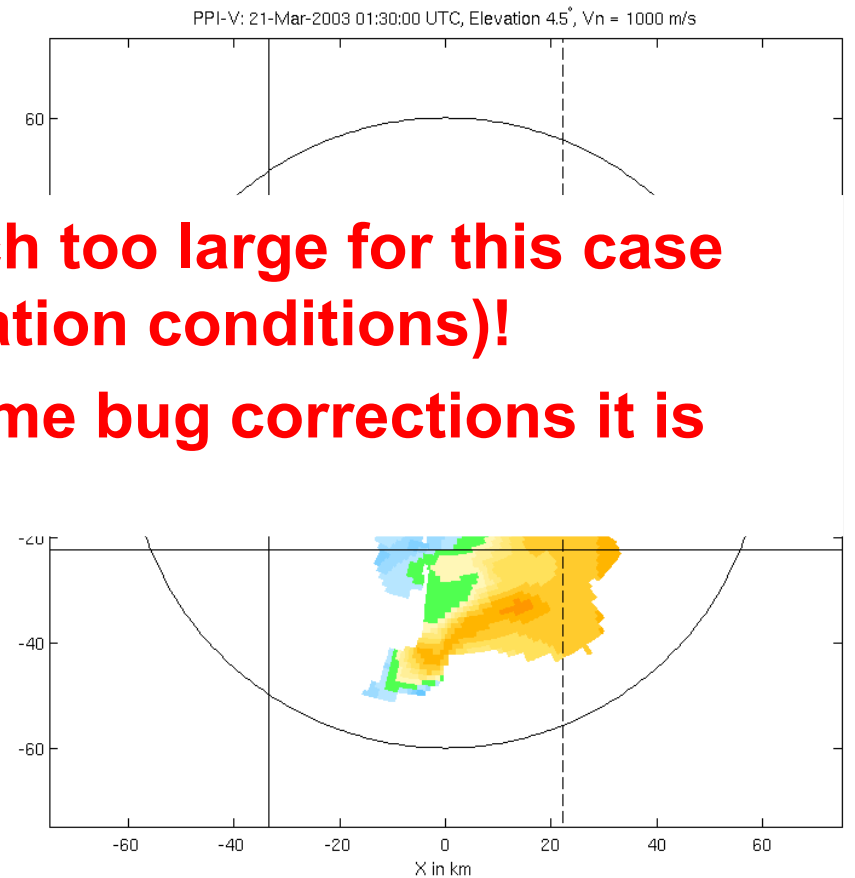
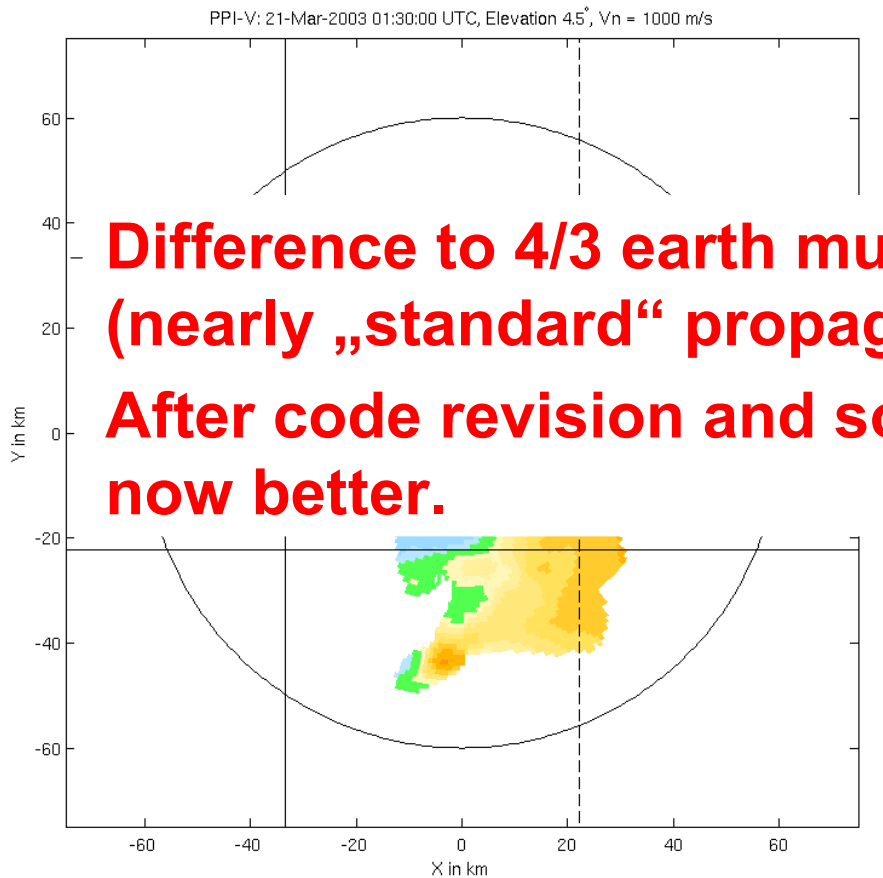
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Results idealized convection 1 km

Radial wind

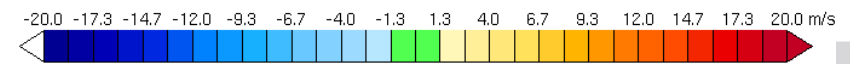
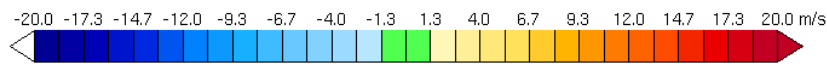
Online propag., no smoothing

Online propag., vertical smoothing



Difference to 4/3 earth much too large for this case (nearly „standard“ propagation conditions)!

After code revision and some bug corrections it is now better.



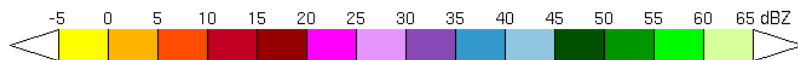
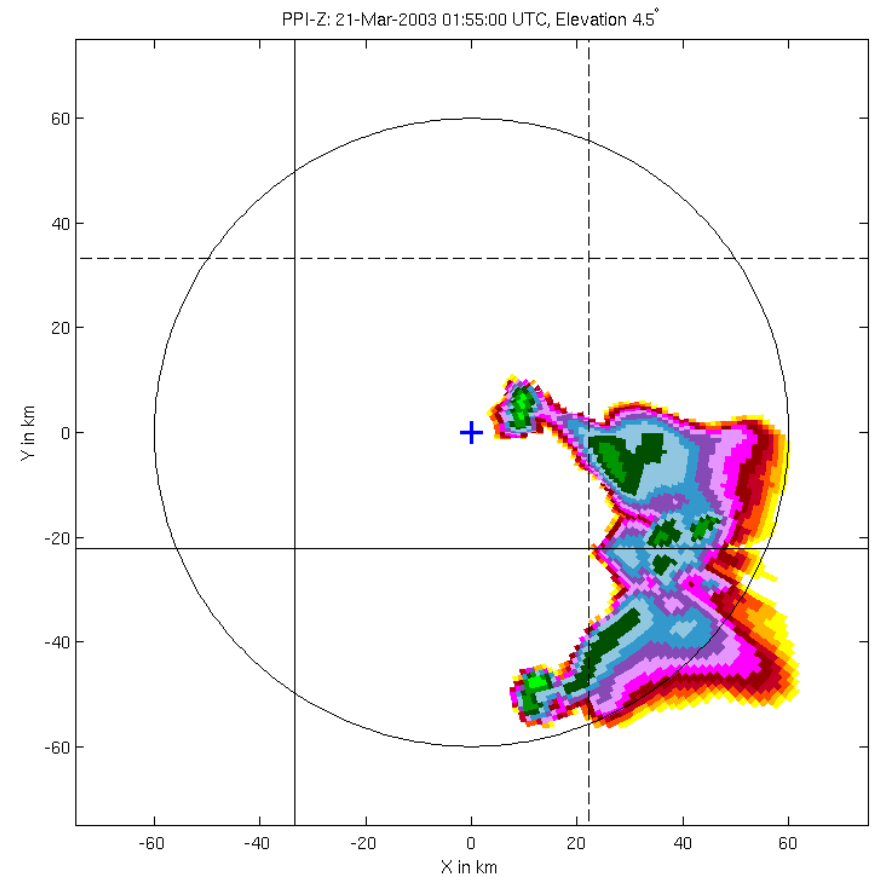
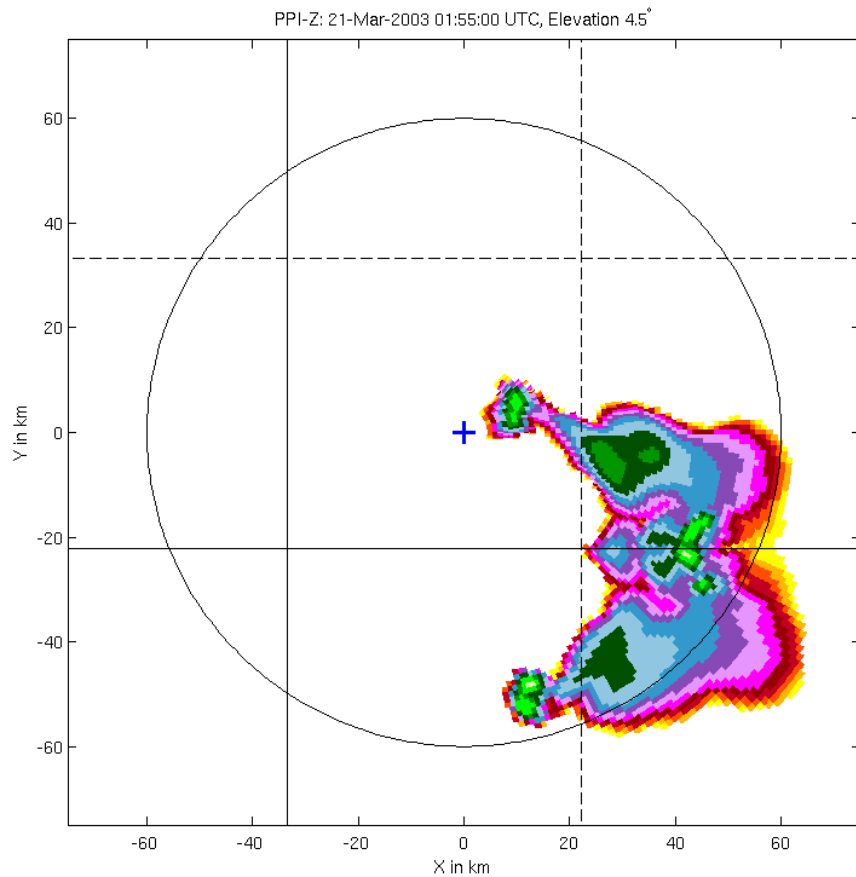
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Results idealized convection 1 km

Reflectivity @ wavelength **5.5 cm**

Simple Rayleigh approx. no attenuation

Mie scattering + attenuation



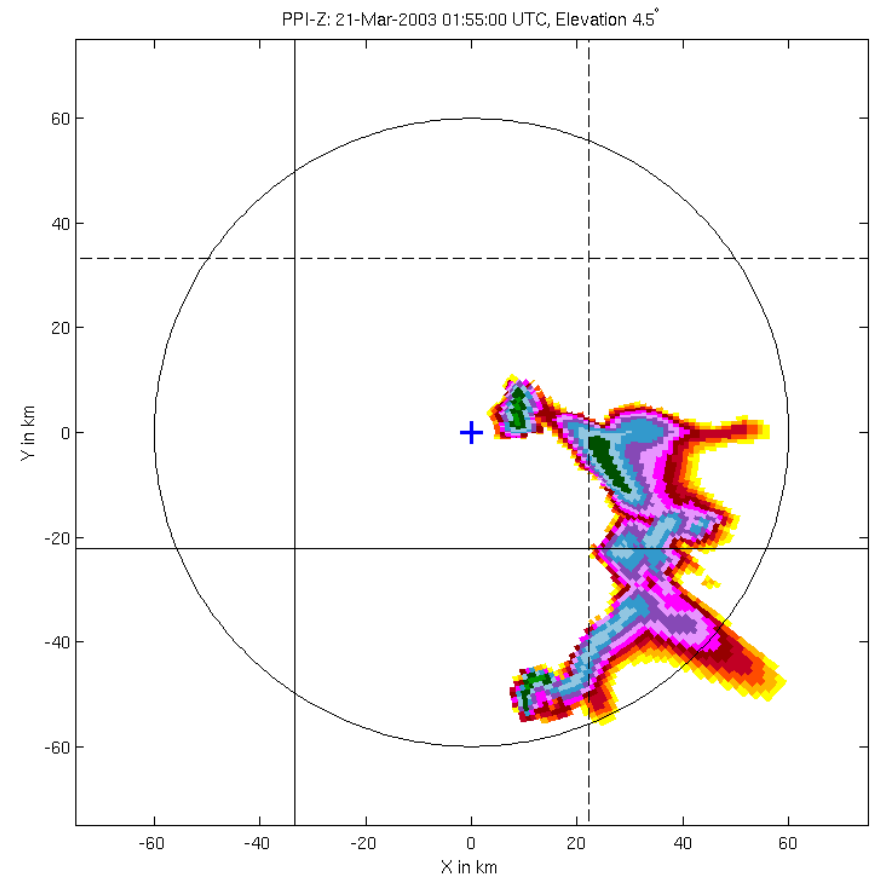
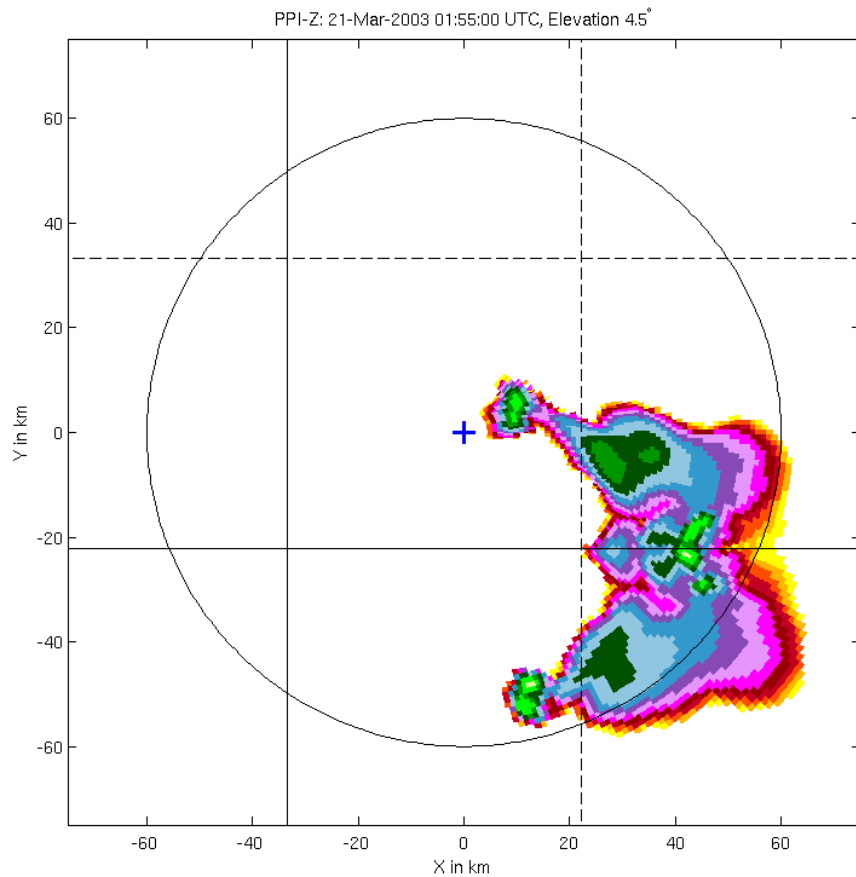
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Results idealized convection 1 km

Reflectivity @ wavelength **3.0 cm**

Simple Rayleigh approx. no attenuation

Mie scattering + attenuation



Efficiency @ 1 km resol.

(version with online propag. calculations)

Subroutine	Vectorization degree [%] and CPU time [s]			
	Without space averaging		With space averaging	
calc_geometry_grid	97.63%	0.019s(\cong 0.0%)	97.63%	0.019s(\cong 0.0%)
calc_grd_rfridx	99.91%	0.229s(\cong 0.0%)	99.91%	0.219s(\cong 0.0%)
calc_grd_winduvw	99.78%	0.374s(\cong 0.0%)	99.78%	0.376s(\cong 0.0%)
calc_grd_reflectivity	99.34%	0.330s(\cong 0.0%)	99.34%	0.326s(\cong 0.0%)
calc_geometry_online	85.39%	8.539s(\cong 0.2%)	84.30%	48.89s(\cong 1.1%)
calc_mod_radialwind_online	99.58%	0.461s(\cong 0.0%)	99.81%	1.771s(\cong 0.1%)
calc_mod_reflectivity_online	99.60%	0.221s(\cong 0.0%)	99.81%	0.801s(\cong 0.0%)
output_radar	91.29%	3.512s(\cong 0.1%)	97.58%	6.063s(\cong 0.1%)
communication expenses	> 1319s(\cong 30.6%)		> 1281s(\cong 30.2%)	
total CPU time	4217.903s		4243.724s	

actual Ze-calc. (Mie-scattering) is done elsewhere and hides in the „communication expenses“ (load imbalance)!

Efficiency @ 1 km resol.

For both online propag. and 4/3 earth model:

- Communication amount for online propag. higher, but not so critical (might be different for 2.8 km !)
- „Bottleneck“: Mie-scattering in combination with load imbalance causes long „waiting times“ for idle processors

In consequence:

- Optimization of the scattering parameter calculations on the model grid necessary.

Easiest way: (regular) lookup tables, computed only once at model start, (multi-)linear table interpolation.

First: reflectivity lookup tables, later similar concept for polarisation parameters.

Weitergehende Fragestellungen

- **Wie kann man Modellverifikation mittels 3D Radardaten betreiben? Was kann man gewinnen?**
- **Assimilation von Radardaten: wie reagiert das Modell auf die Assimilation solcher Massendaten? Wo liegen die Probleme? Was kann man gewinnen?**
- **Abschätzung von Effekten der nichtgleichmäßigen Strahlfüllung auf Dämpfung (k²-Ze-Beziehung).**

Radial wind operator

$$\langle v_r^{(R)} \rangle = \frac{\int_{r_0-\Delta r/2}^{r_0+\Delta r/2} \int_{-\pi}^{\pi} \int_{-\pi/2}^{\pi/2} \left(\int_0^{\infty} \sigma_b(D) N(D, r, \phi, \theta) [(\vec{v} - v_T(D)\vec{e}_3) \cdot \vec{e}_r] dD \right) \frac{f(\phi, \theta)^4}{r^2} \cos \theta d\theta d\phi dr}{\int_{r_0-\Delta r/2}^{r_0+\Delta r/2} \int_{-\pi}^{\pi} \int_{-\pi/2}^{\pi/2} \eta(r, \phi, \theta) \frac{f(\phi, \theta)^4}{r^2} \cos \theta d\theta d\phi dr}$$

$$= \frac{\int_{r_0-\Delta r/2}^{r_0+\Delta r/2} \int_{-\pi}^{\pi} \int_{-\pi/2}^{\pi/2} (\vec{v} \cdot \vec{e}_r) \frac{\eta}{l_n^2} \frac{f^4}{r^2} \cos(\theta) d\theta d\phi dr}{\int_{r_0-\Delta r/2}^{r_0+\Delta r/2} \int_{-\pi}^{\pi} \int_{-\pi/2}^{\pi/2} \frac{\eta}{l_n^2} \frac{f^4}{r^2} \cos(\theta) d\theta d\phi dr} - \frac{\int_{r_0-\Delta r/2}^{r_0+\Delta r/2} \int_{-\pi}^{\pi} \int_{-\pi/2}^{\pi/2} \left(\vec{e}_3 \cdot \vec{e}_r \int_0^{\infty} \sigma_b(D) N(D) v_T(D) dD \right) \frac{1}{l_n^2} \frac{f^4}{r^2} \cos(\theta) d\theta d\phi dr}{\int_{r_0-\Delta r/2}^{r_0+\Delta r/2} \int_{-\pi}^{\pi} \int_{-\pi/2}^{\pi/2} \frac{\eta}{l_n^2} \frac{f^4}{r^2} \cos(\theta) d\theta d\phi dr}$$

$$= \frac{\int_{r_0-\Delta r/2}^{r_0+\Delta r/2} \int_{-\pi}^{\pi} \int_{-\pi/2}^{\pi/2} (\vec{v} \cdot \vec{e}_r) \frac{\eta}{l_n^2} \frac{f^4}{r^2} \cos(\theta) d\theta d\phi dr}{\int_{r_0-\Delta r/2}^{r_0+\Delta r/2} \int_{-\pi}^{\pi} \int_{-\pi/2}^{\pi/2} \frac{\eta}{l_n^2} \frac{f^4}{r^2} \cos(\theta) d\theta d\phi dr} - \frac{\int_{r_0-\Delta r/2}^{r_0+\Delta r/2} \int_{-\pi}^{\pi} \int_{-\pi/2}^{\pi/2} (\vec{e}_3 \cdot \vec{e}_r) \bar{v}_T \frac{\eta}{l_n^2} \frac{f^4}{r^2} \cos(\theta) d\theta d\phi dr}{\int_{r_0-\Delta r/2}^{r_0+\Delta r/2} \int_{-\pi}^{\pi} \int_{-\pi/2}^{\pi/2} \frac{\eta}{l_n^2} \frac{f^4}{r^2} \cos(\theta) d\theta d\phi dr}$$

■ Aufzählung

- asdfasdf
- asfdasdf

■ Zweiter Punkt

- asdfasdf
- asdasdf