

Parameterization of free and
forced convection in the
atmospheric boundary layer
based on large-eddy simulations

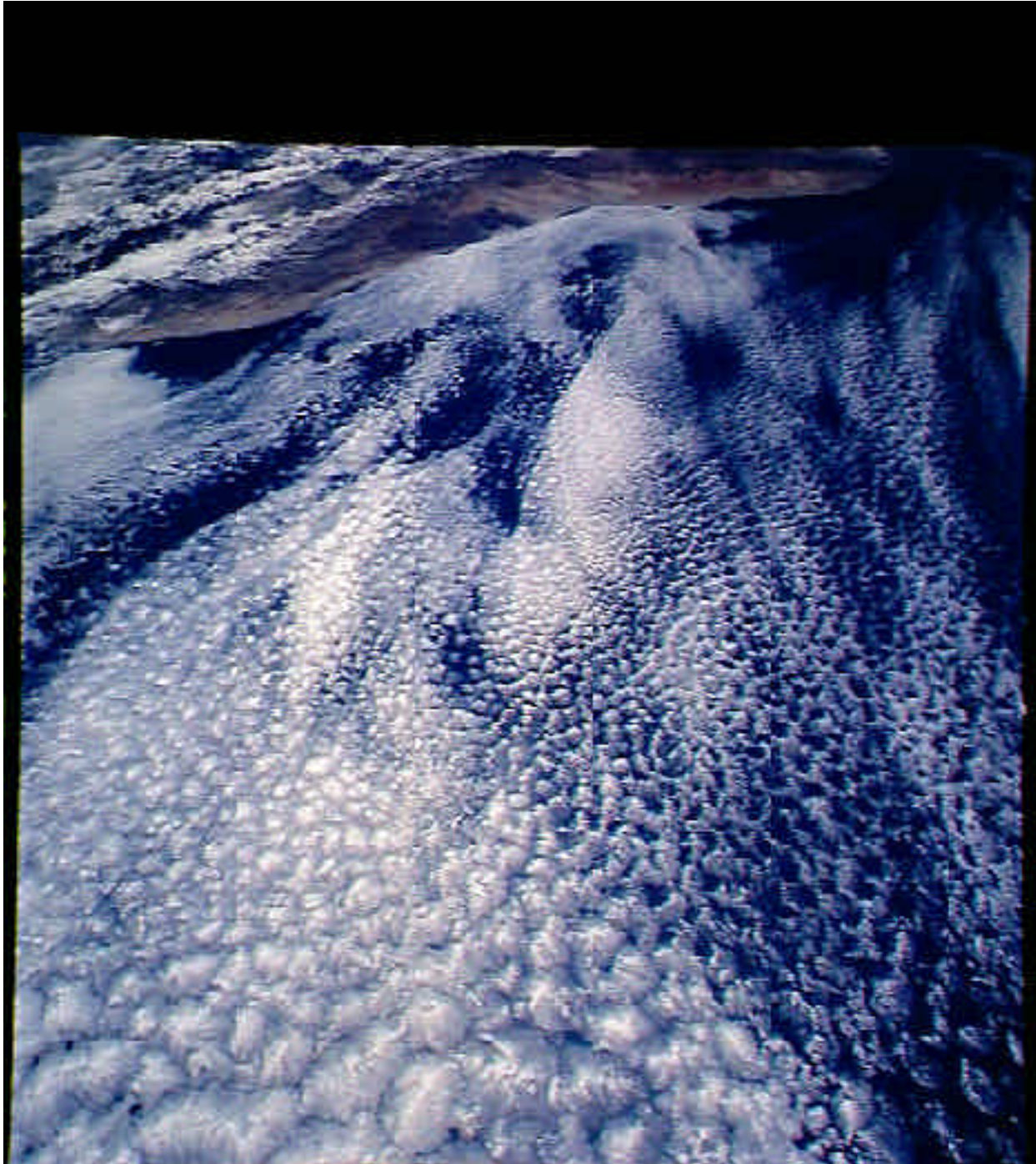
Zbigniew Sorbjan

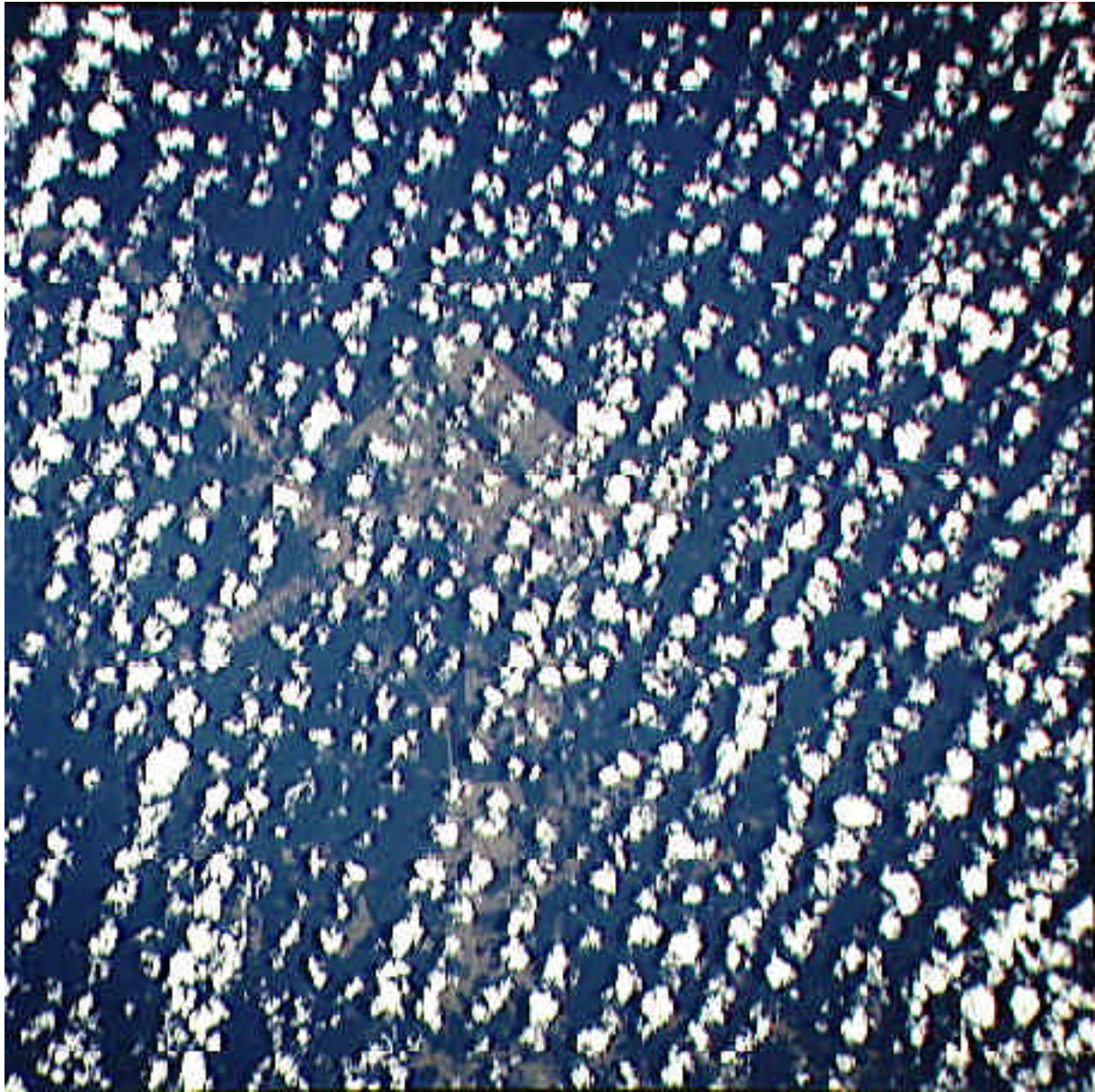
IMGW, Warszawa, Poland

sorbjanz@mu.edu

Forms of atmospheric convection:

- 1. Cloudless free convection (clear cells)
- 2. Cloudless forced convection (clear rolls)
- 3. Cu-topped free convection (open cells)
- 4. Cu-topped forced convection (open rolls)
- 5. Sc-topped free convection (closed cells)
- 6. Sc-topped forced convection (closed rolls)





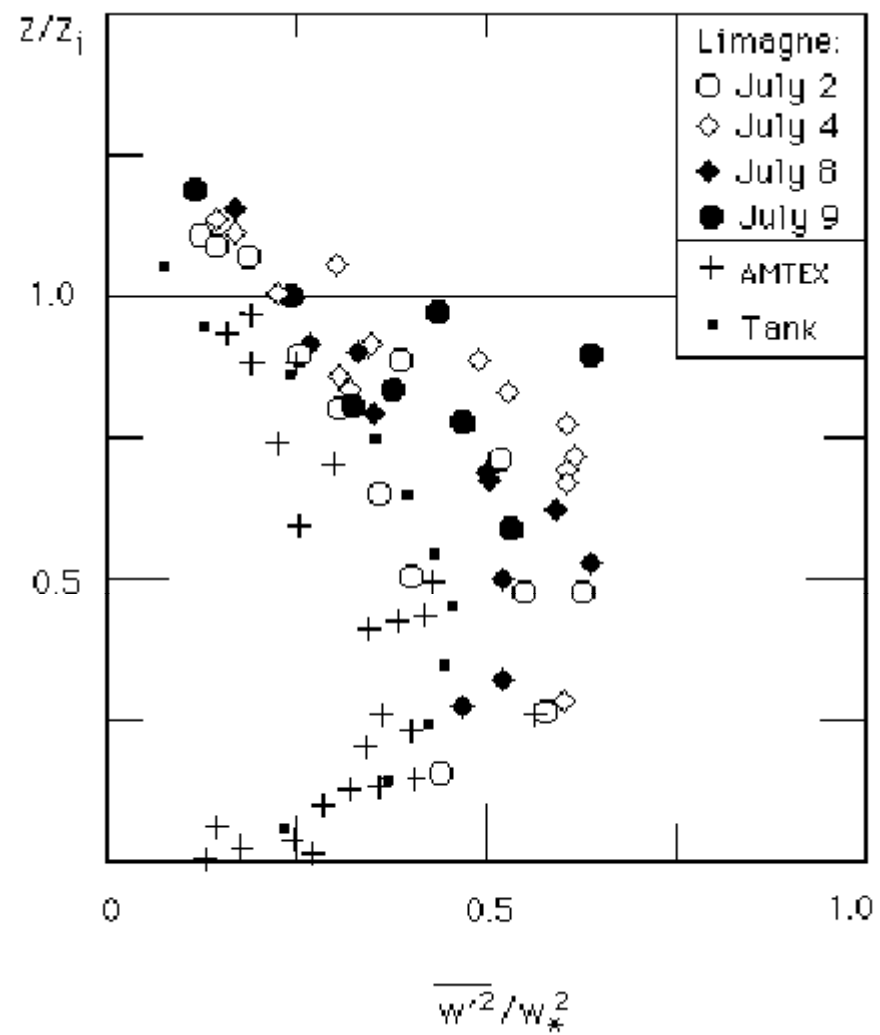
$$w_* = (\beta z_i H_0)^{1/3} \quad \text{for vertical velocity,}$$

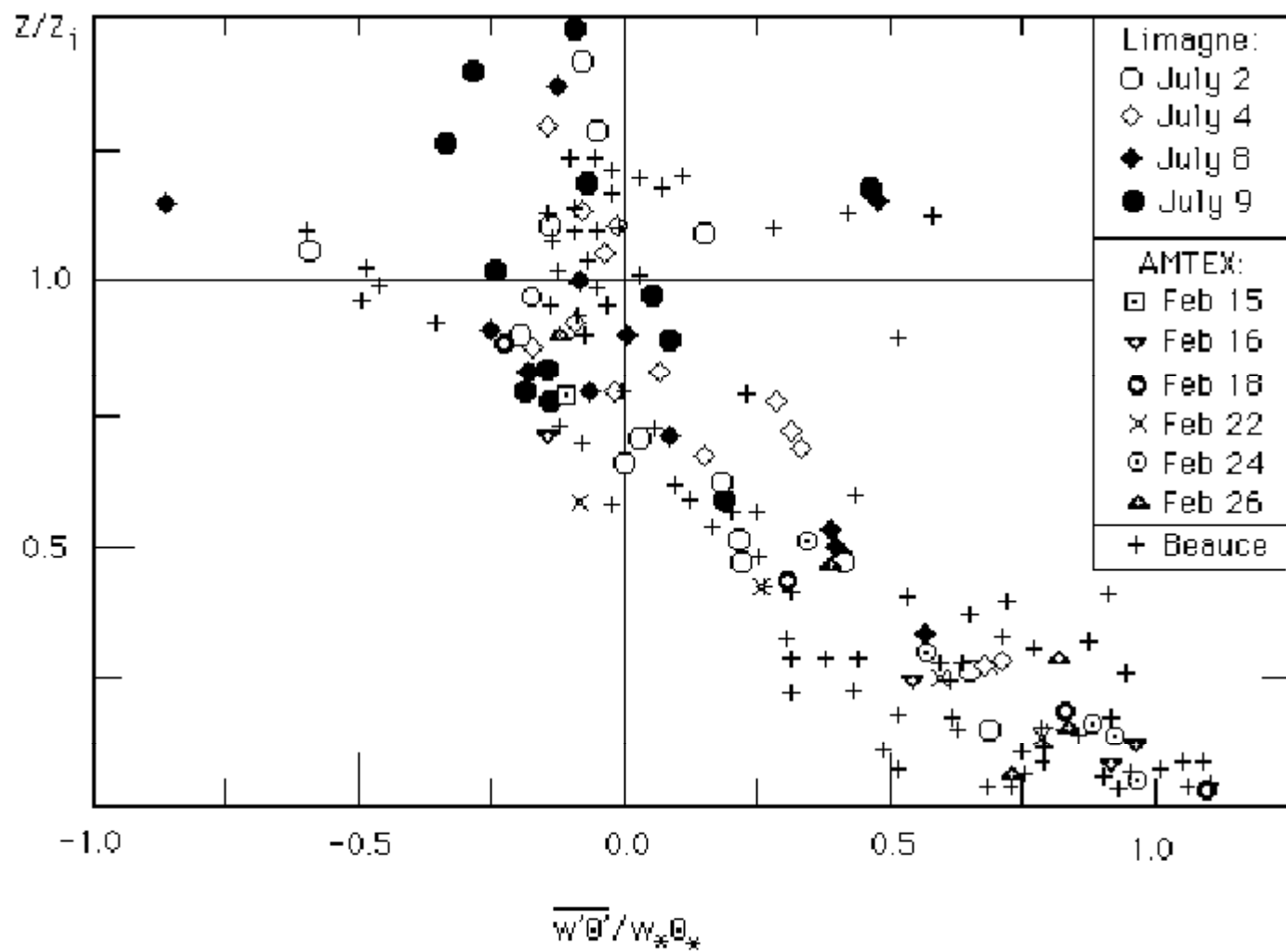
$$\Theta_* = H_0/w_* \quad \text{for temperature,}$$

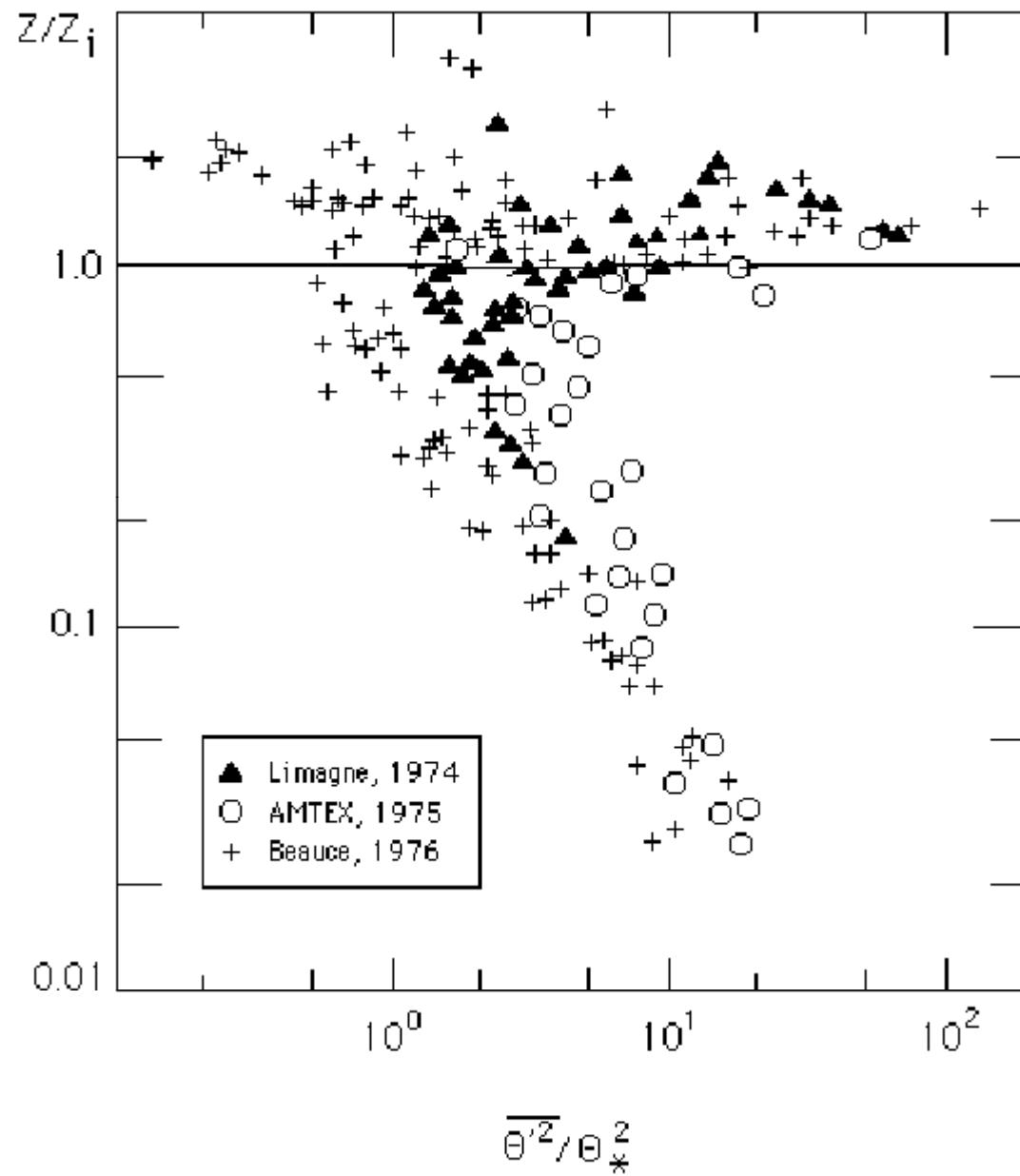
$$q_* = Q/w_* \quad \text{for a passive scalar,}$$

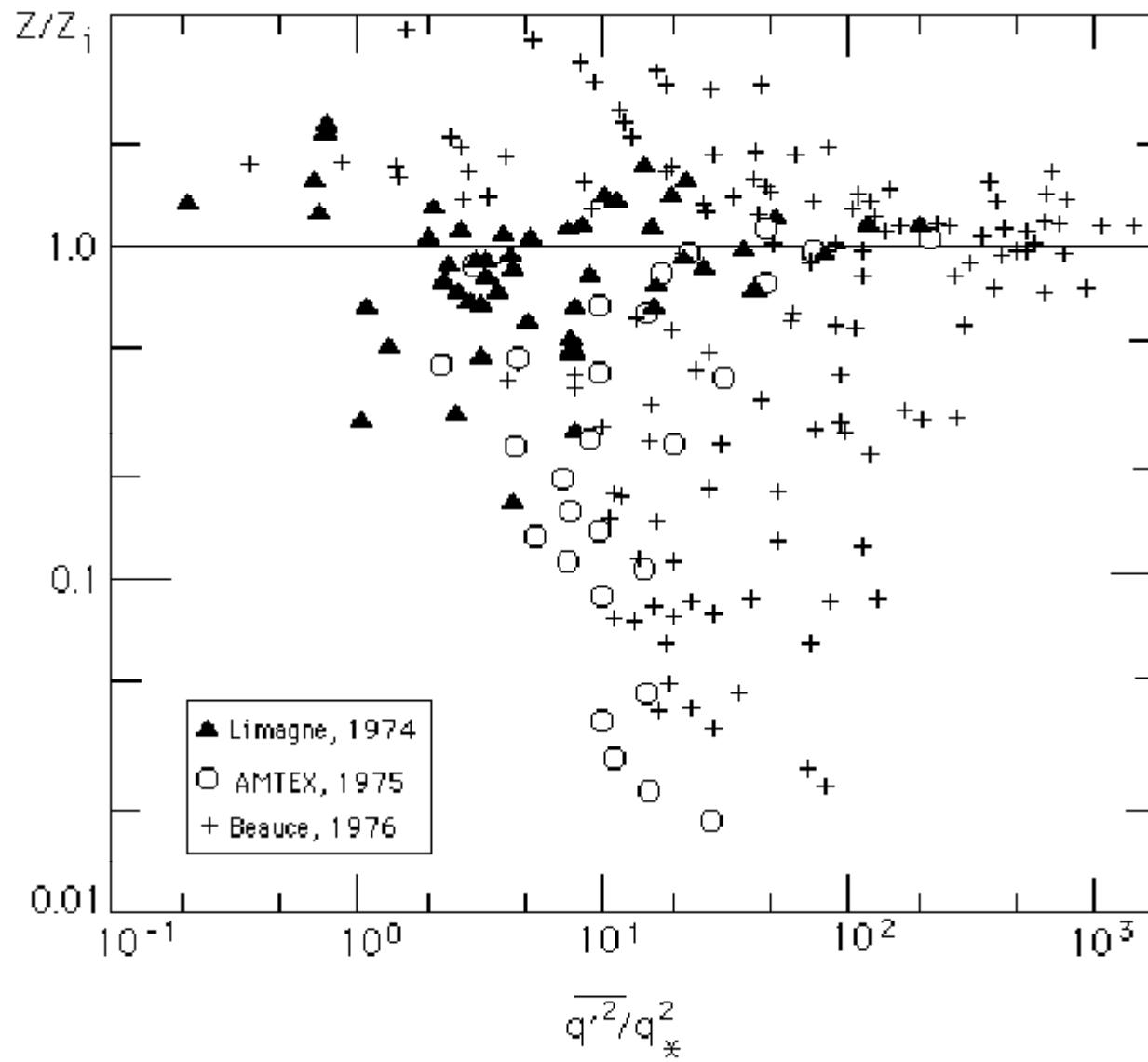
$$z_i \quad \text{for height,}$$

$$\tau_* = w_*/z_i \quad \text{for time,}$$





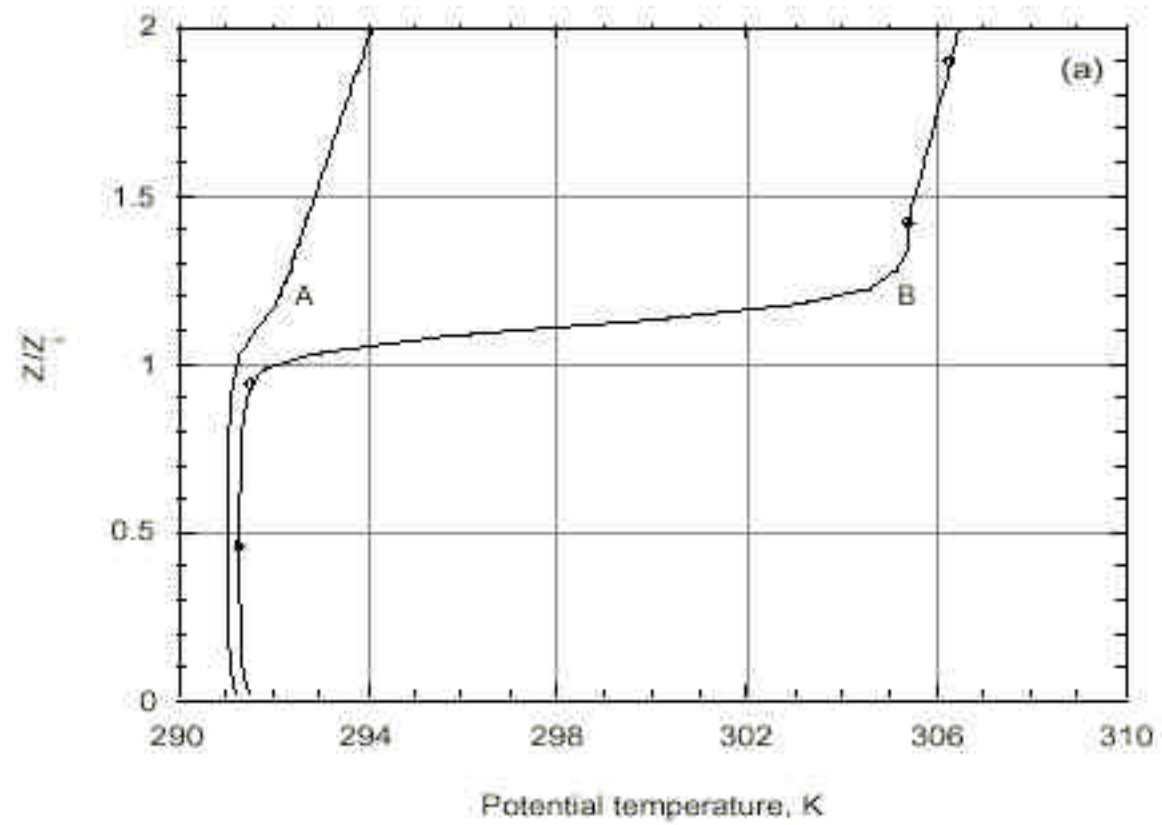


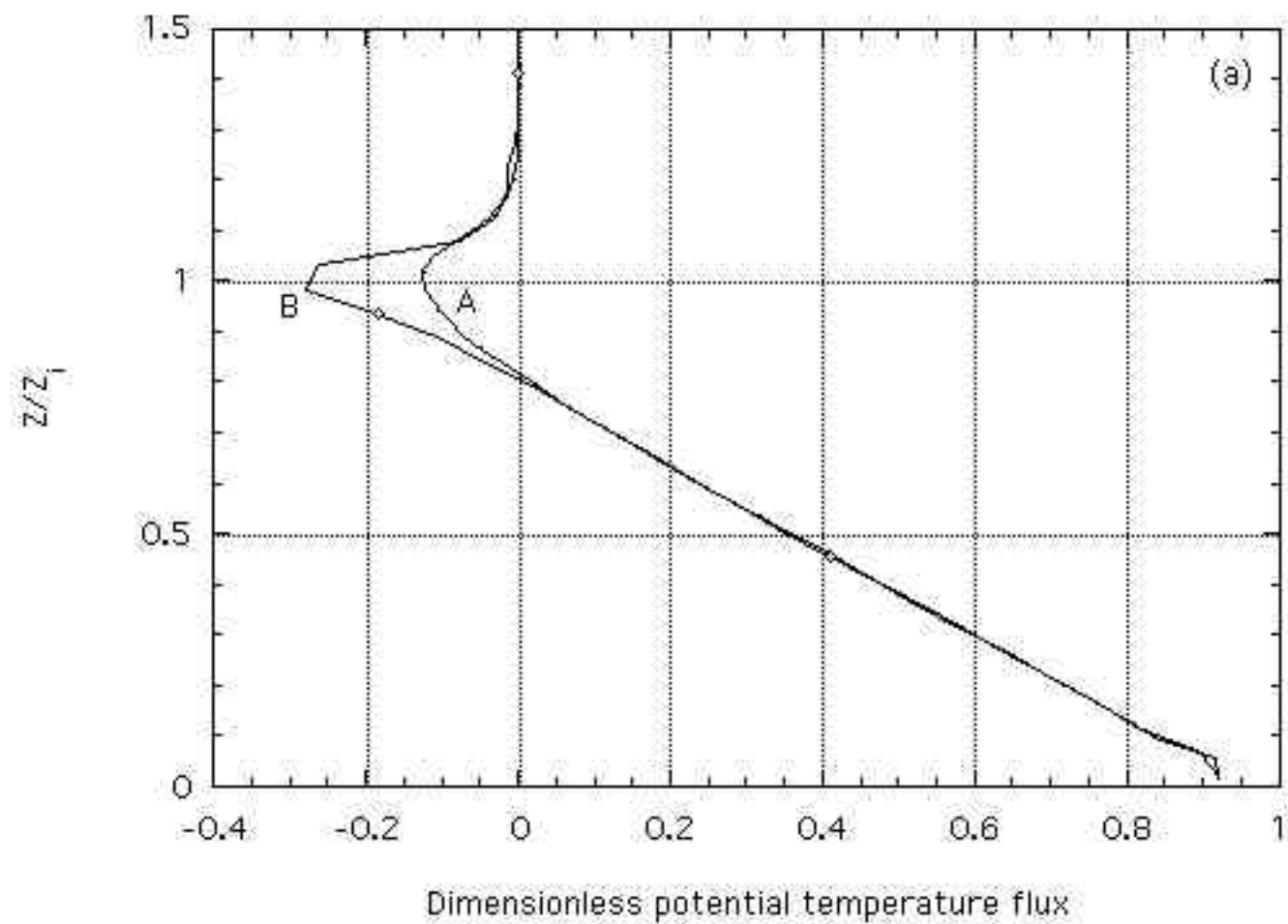


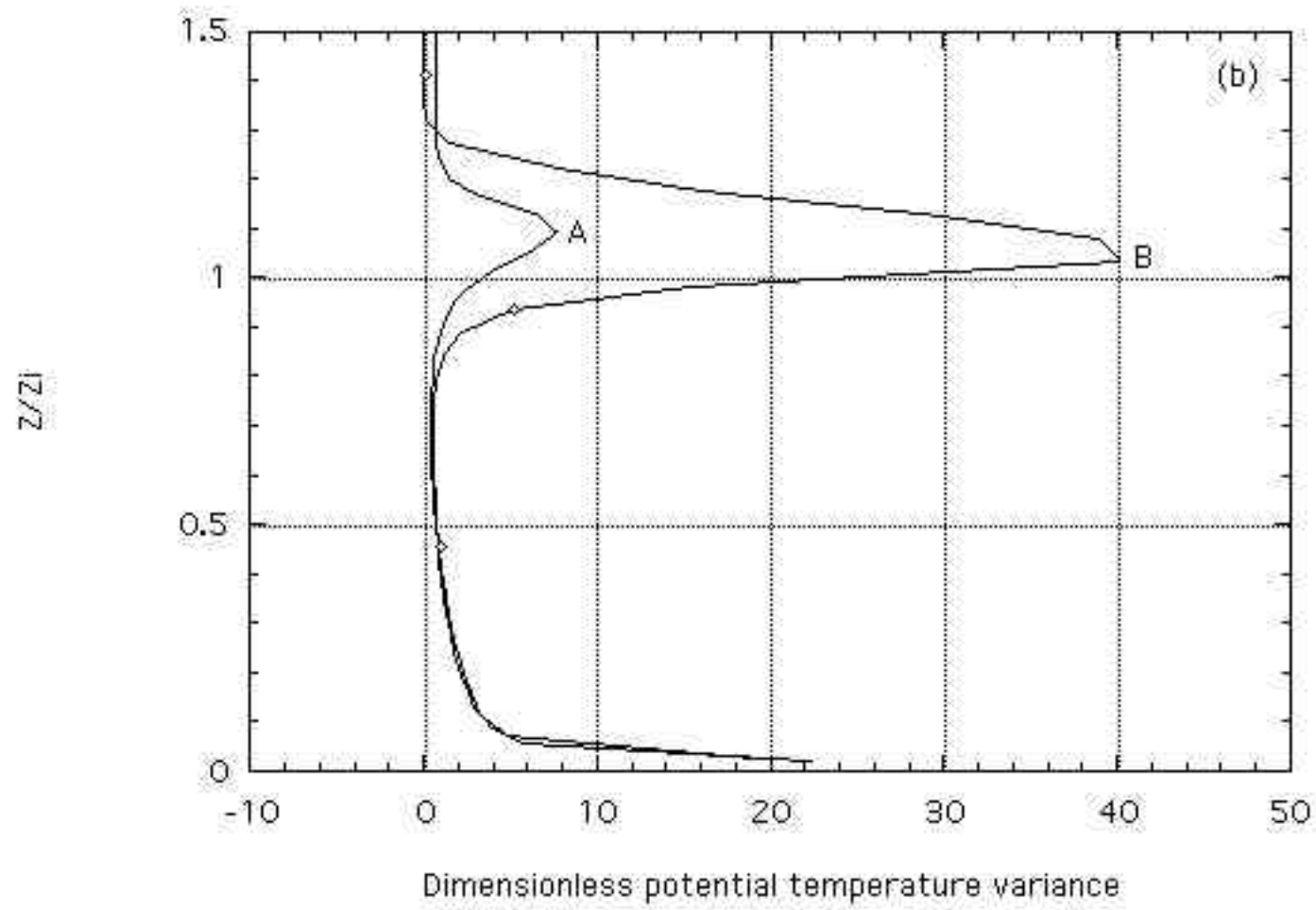
LES experiments:

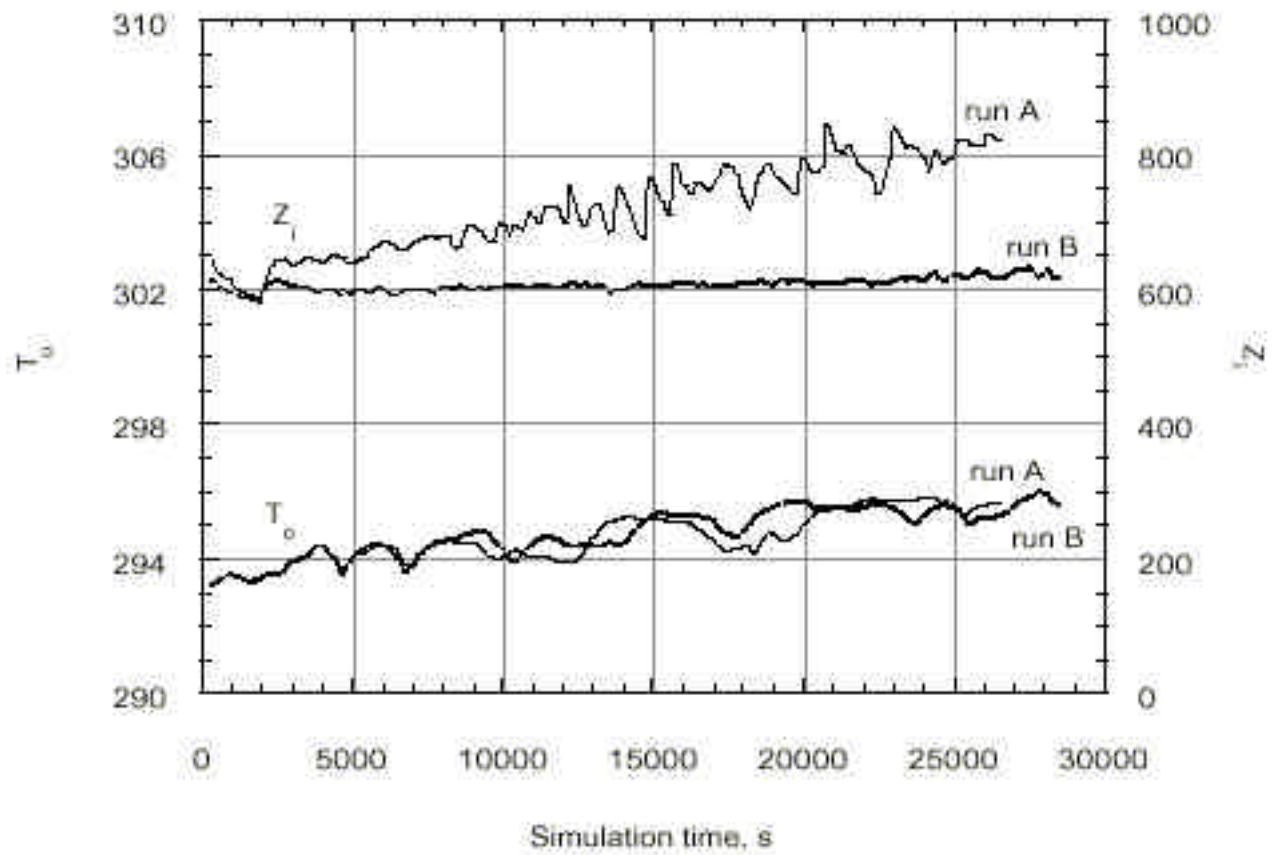
- 1. Free convection
- 2. Forced convection (barotropic)
- 3. Forced convection (baroclinic)

Free-convection experiments









$$S_w = w_* \quad \text{for vertical velocity,}$$

$$S_\theta = w_* N_i / \beta \quad \text{for temperature,}$$

$$S_q = g_i w_* / N_i \quad \text{for humidity (or other scalar),}$$

$$S_h = w_* / N_i \quad \text{for height,}$$

$$S_t = 1 / N_i \quad \text{for time,}$$

where N_i is the Brunt-Vaisala frequency

$$N_i = (\beta \gamma_i)^{0.5}$$

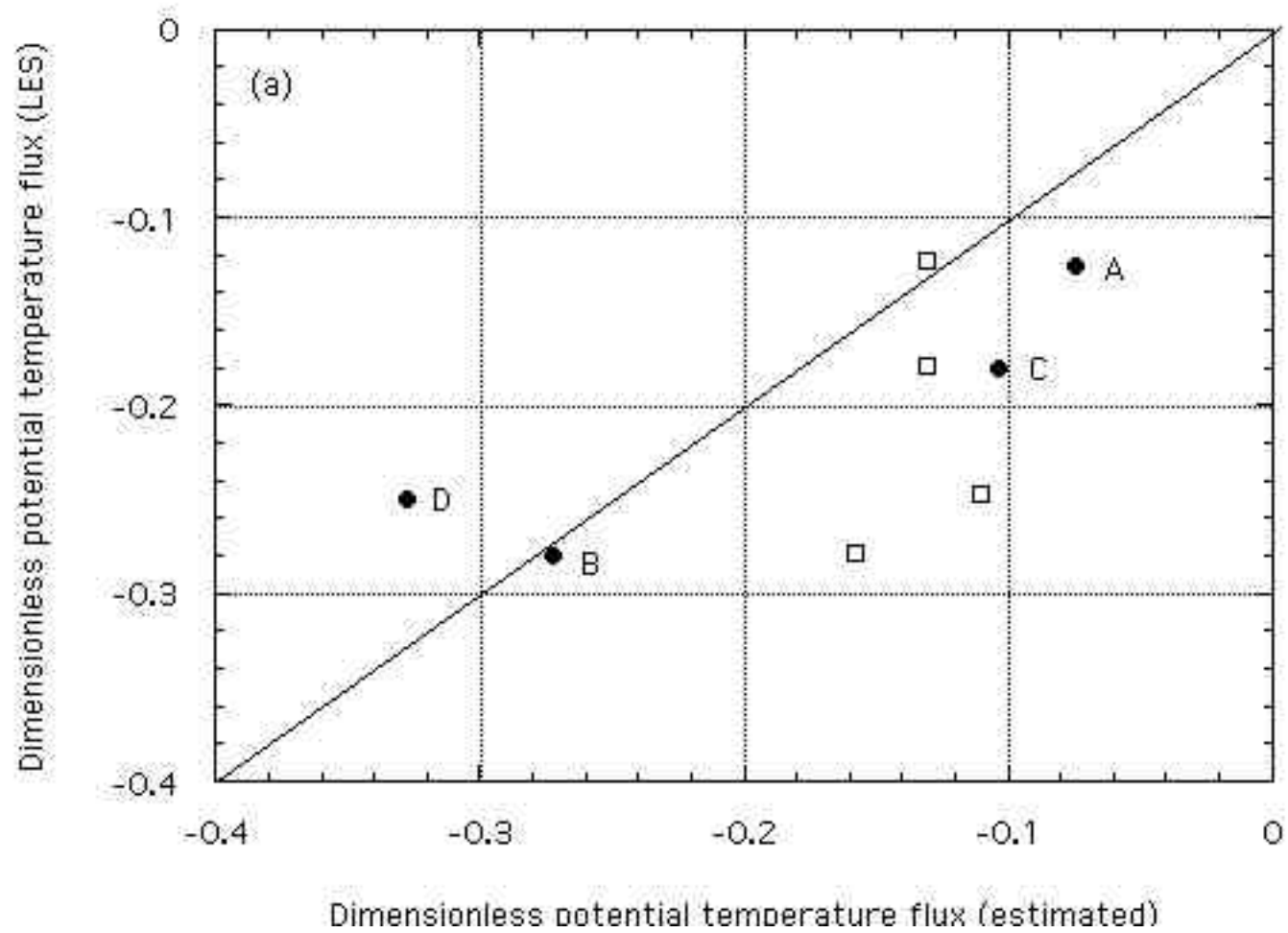
$$H_i = -c_H \sqrt{S} \sqrt{\theta}$$

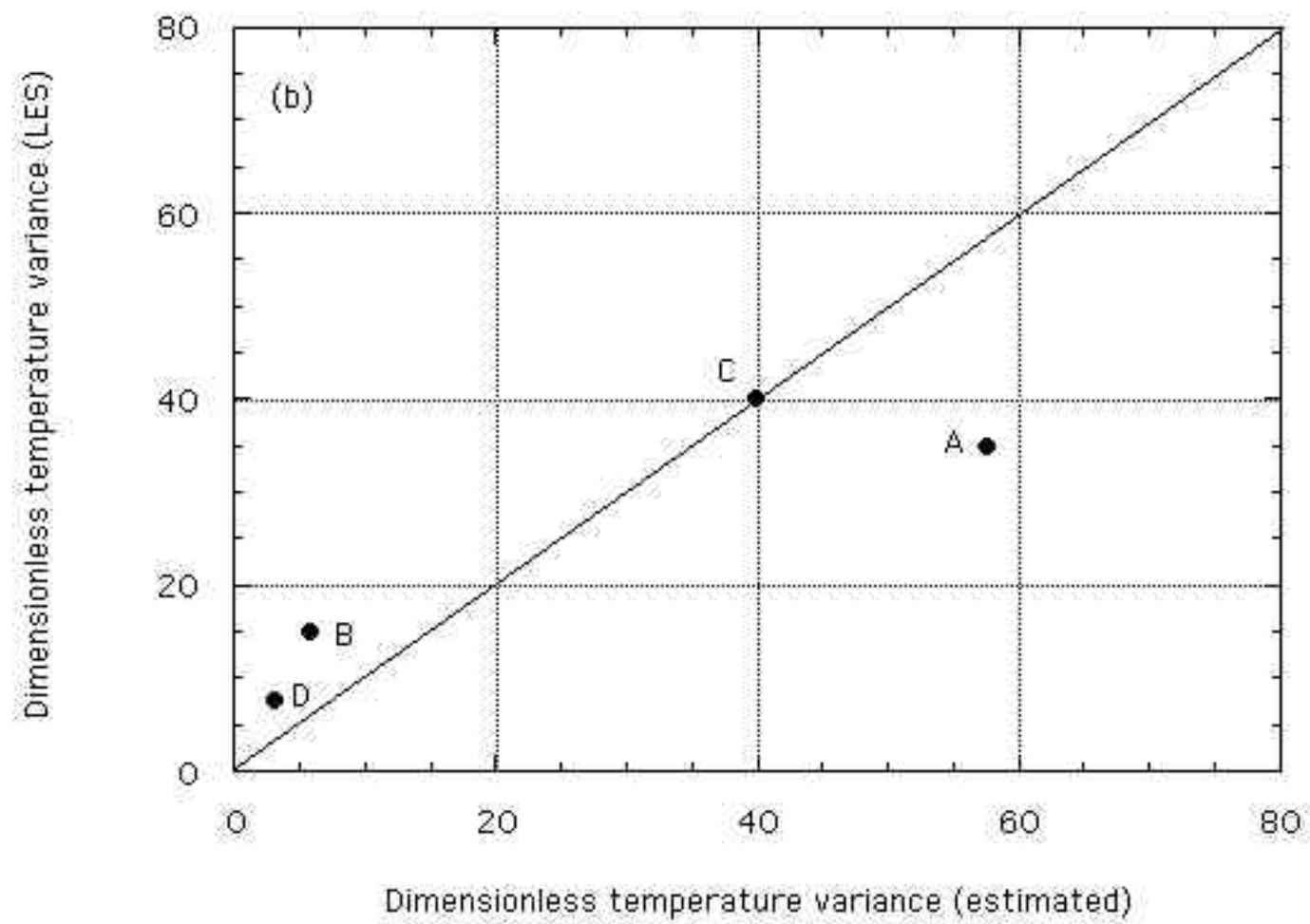
$$Q_i = -c_Q \sqrt{S} \sqrt{q}$$

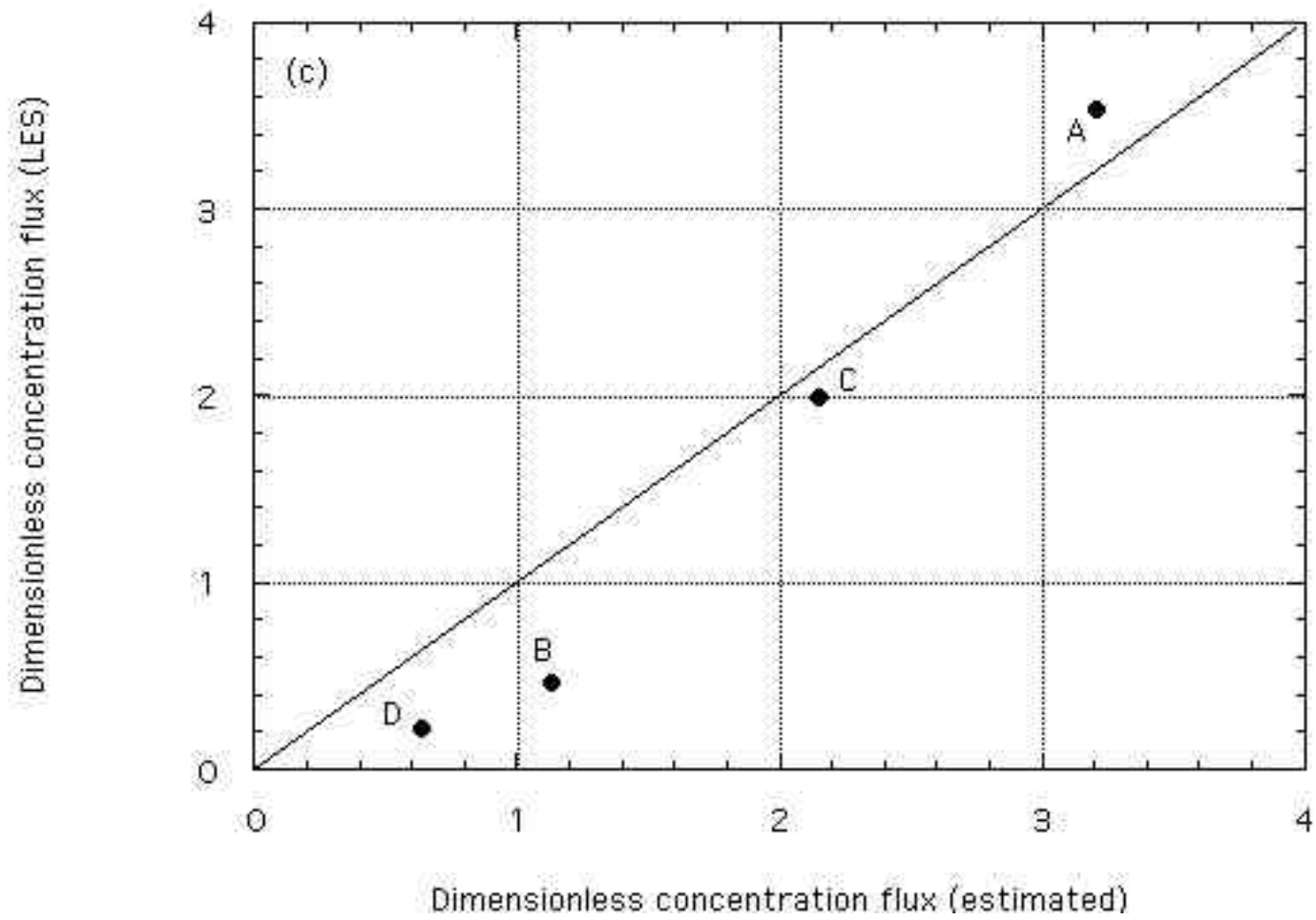
$$\sigma_{\theta i}^2 = \theta c_{\theta}^2 S$$

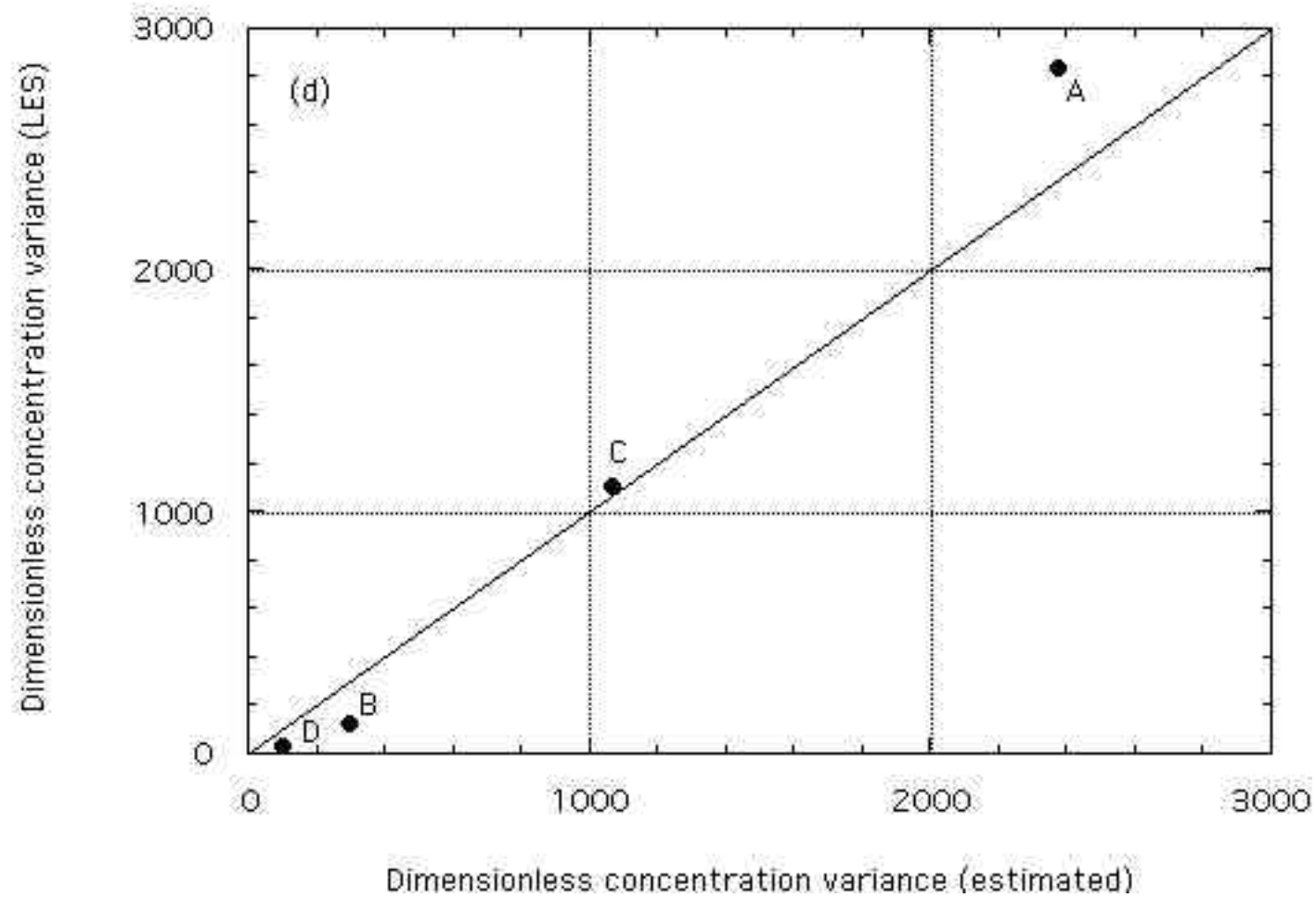
$$\sigma_{qi}^2 = q c_q^2 S$$

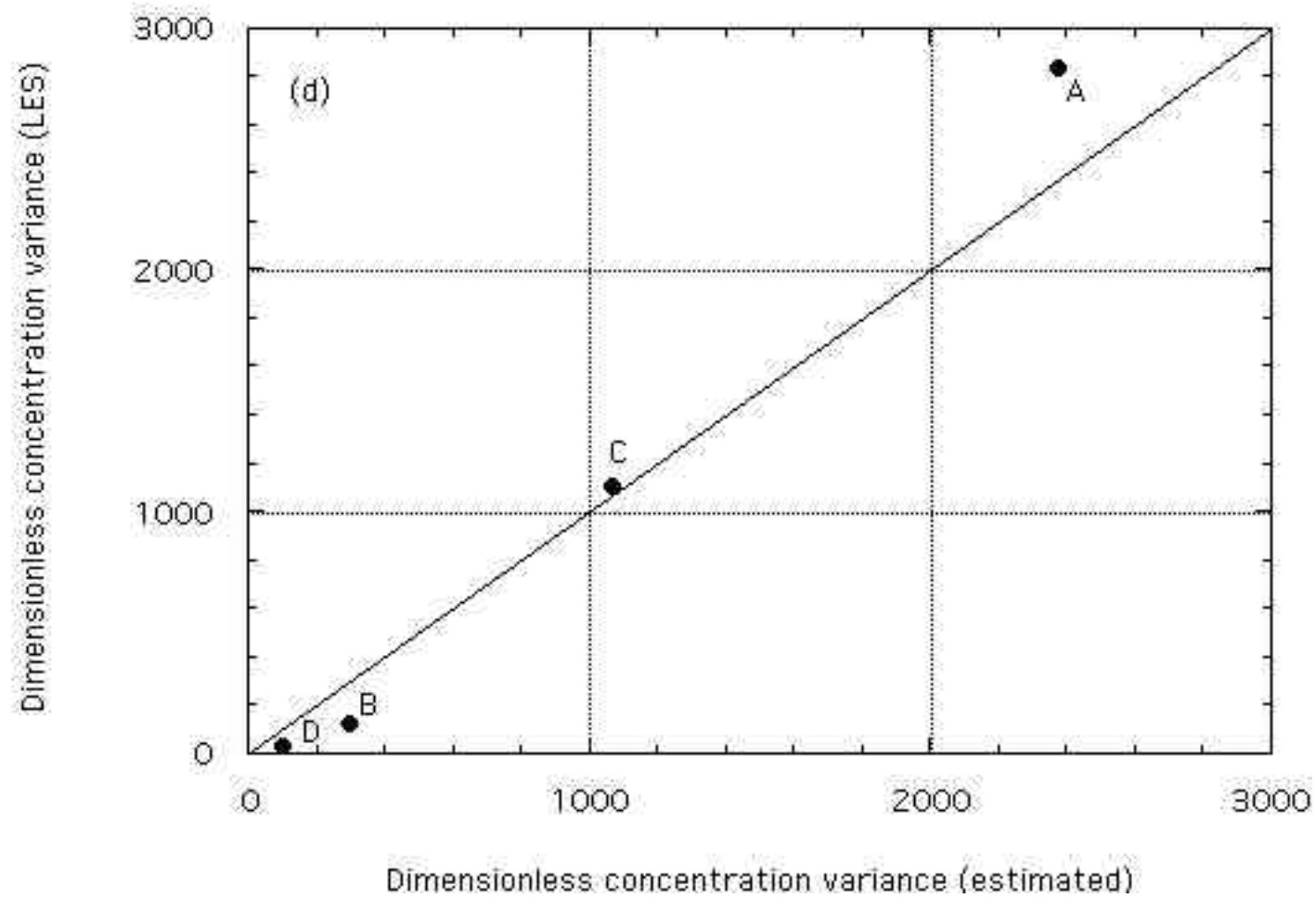
$$C_{\theta qi} = \theta q c_{\theta} c_q S$$



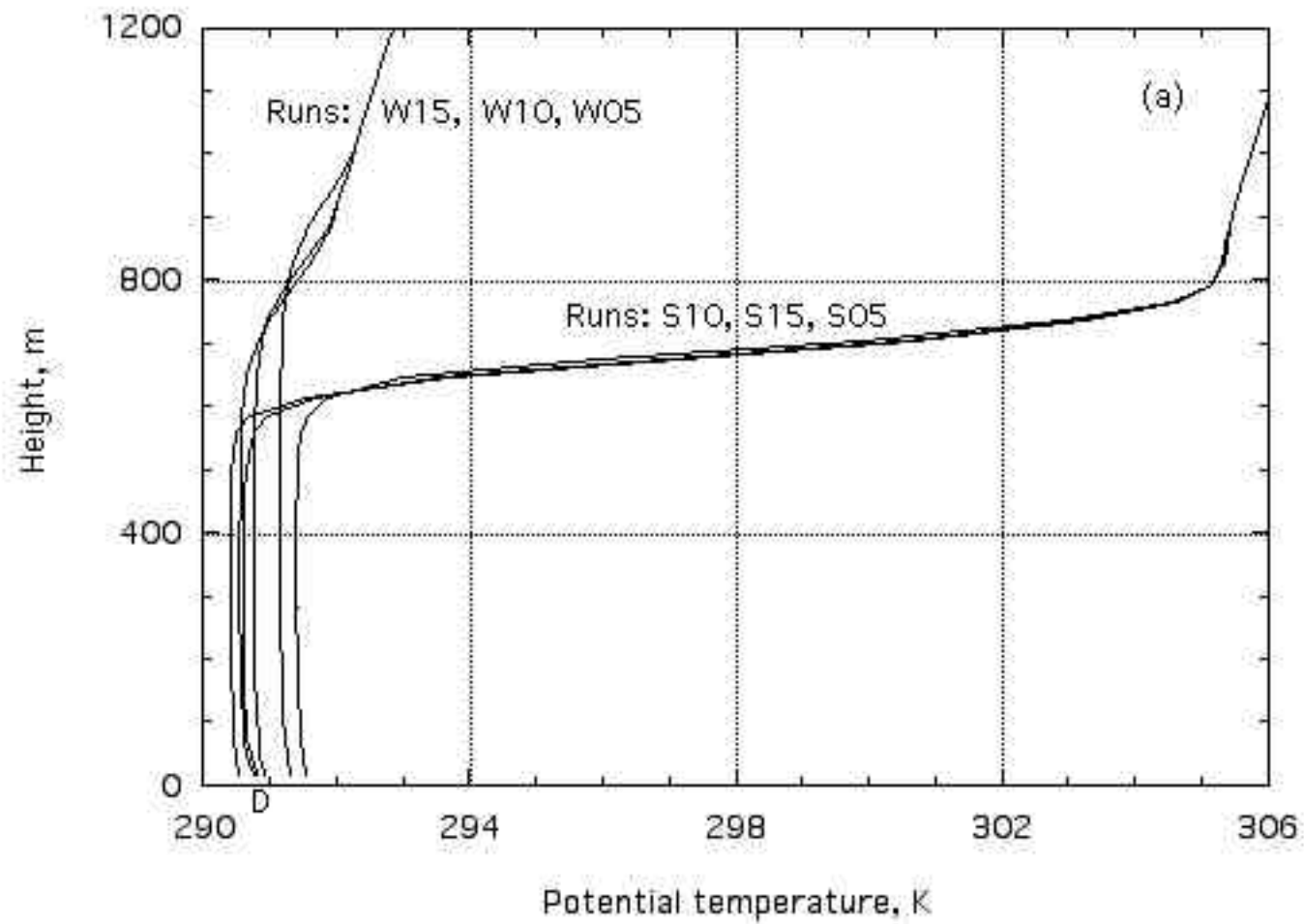


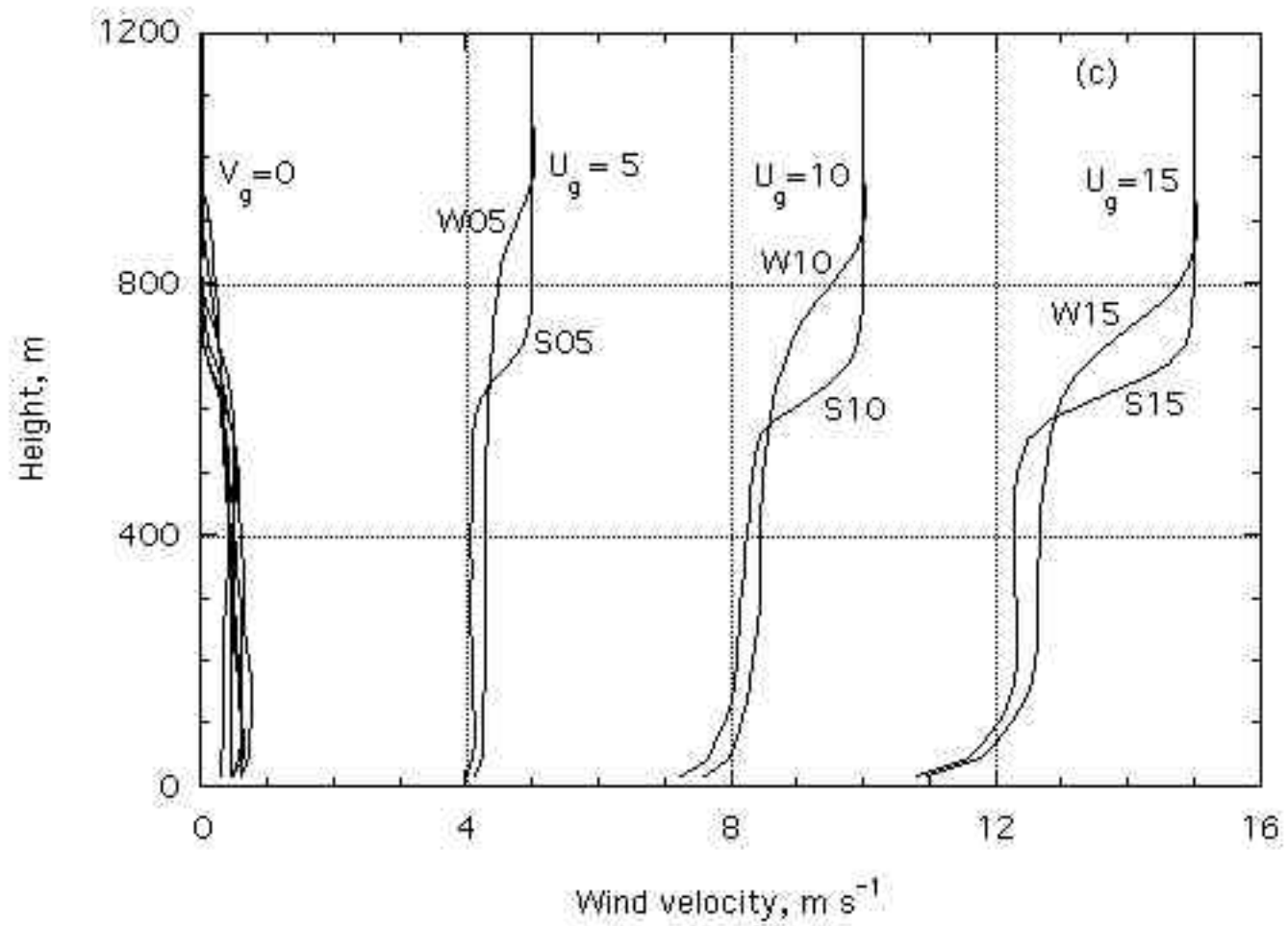






Forced convection
(barotropic)
experiments





When wind shear is present, statistics of turbulence at the top of the mixed layer are dependent not only on the temperature gradient, but also on velocity gradients $s_x = du/dz_1$ and $s_y = dv/dz_1$ in the interfacial layer, equivalently on the interfacial dynamic Richardson number:

$$Ri = \frac{bg}{s_x^2 + s_y^2}$$

$$H_i (S_w/S_\theta) = -c_H (1 + c_r i) / (1 + R)^{1/2} / R i$$

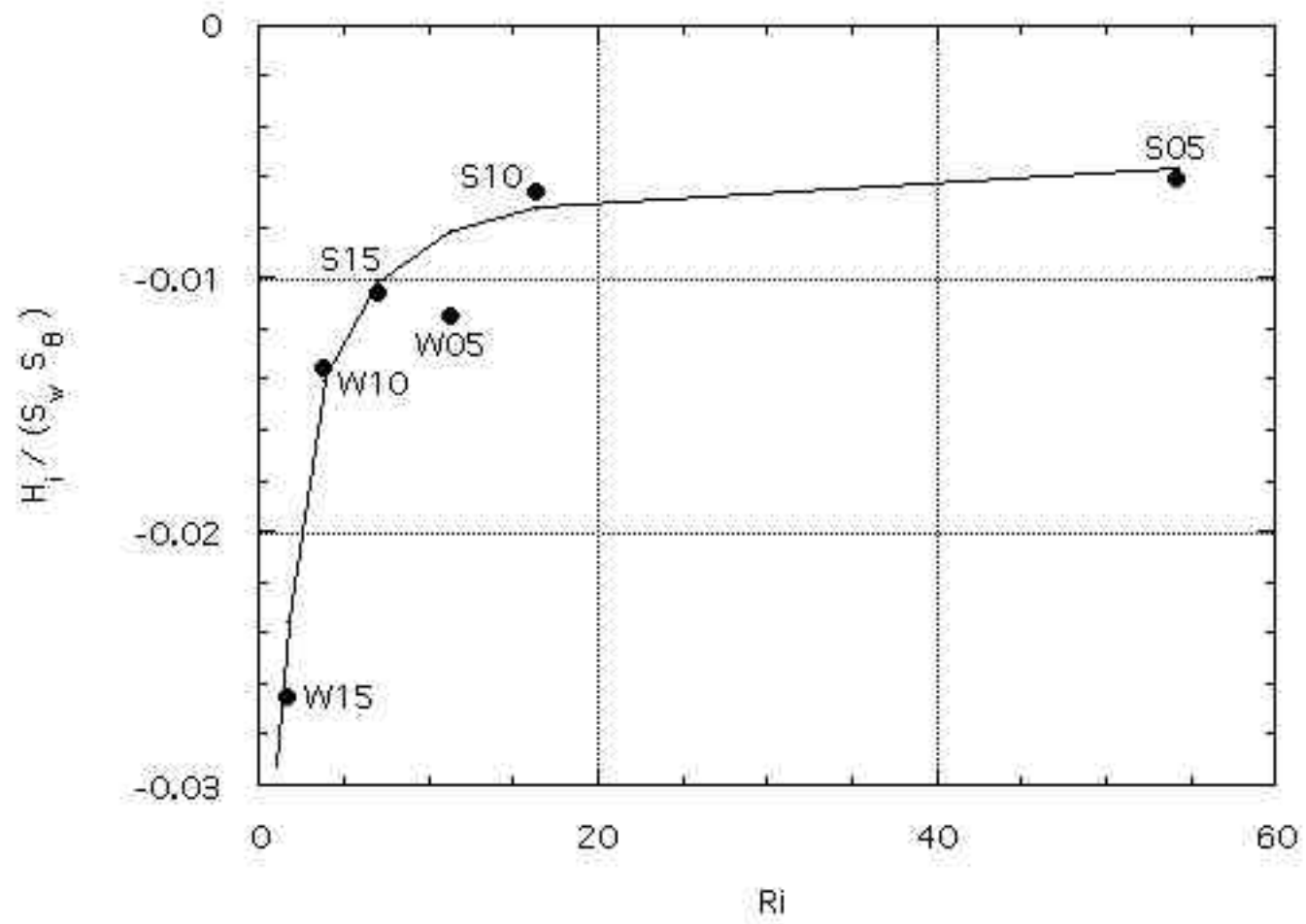
$$Q_i (S_w/S_q) = -c_Q (1 + c_r i) / (1 + R)^{1/2} / R i$$

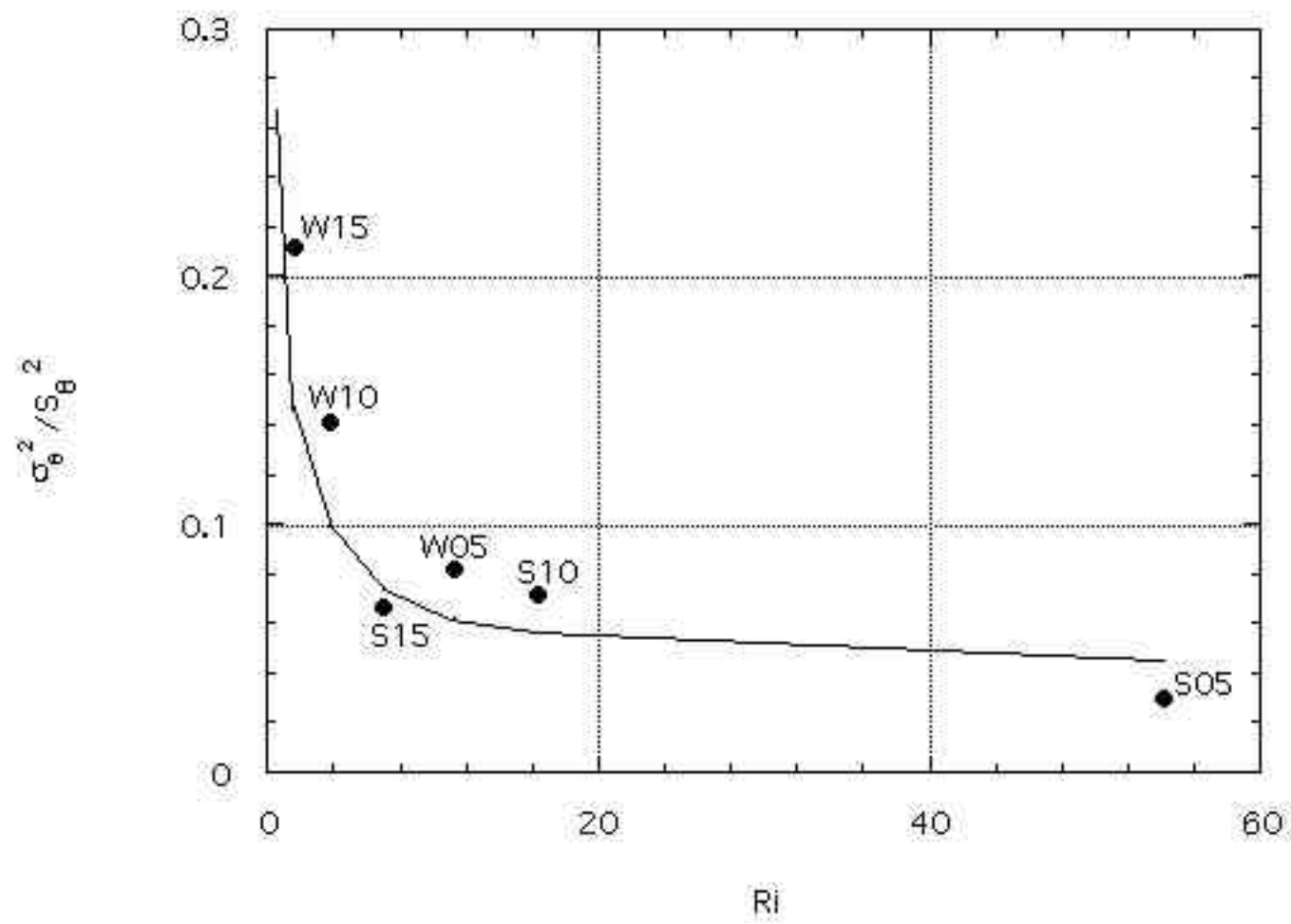
$$\sigma_{\theta i}^2 S_\theta^2 = \theta (1 + c_r ci) / (1 + R) / R i$$

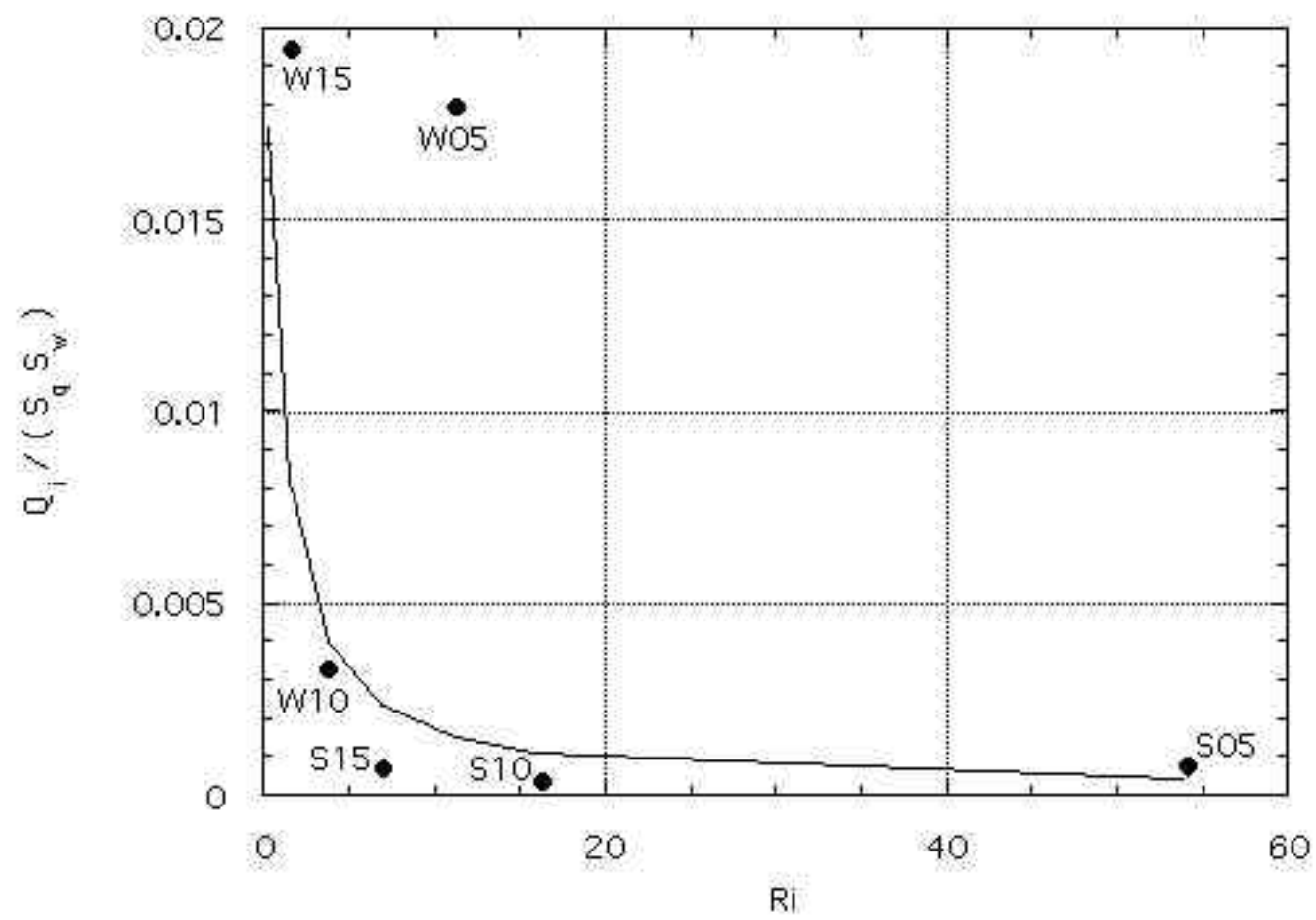
$$\sigma_{qi}^2 S_q^2 / = q (1 + c_r i) / (1 + R) / R i$$

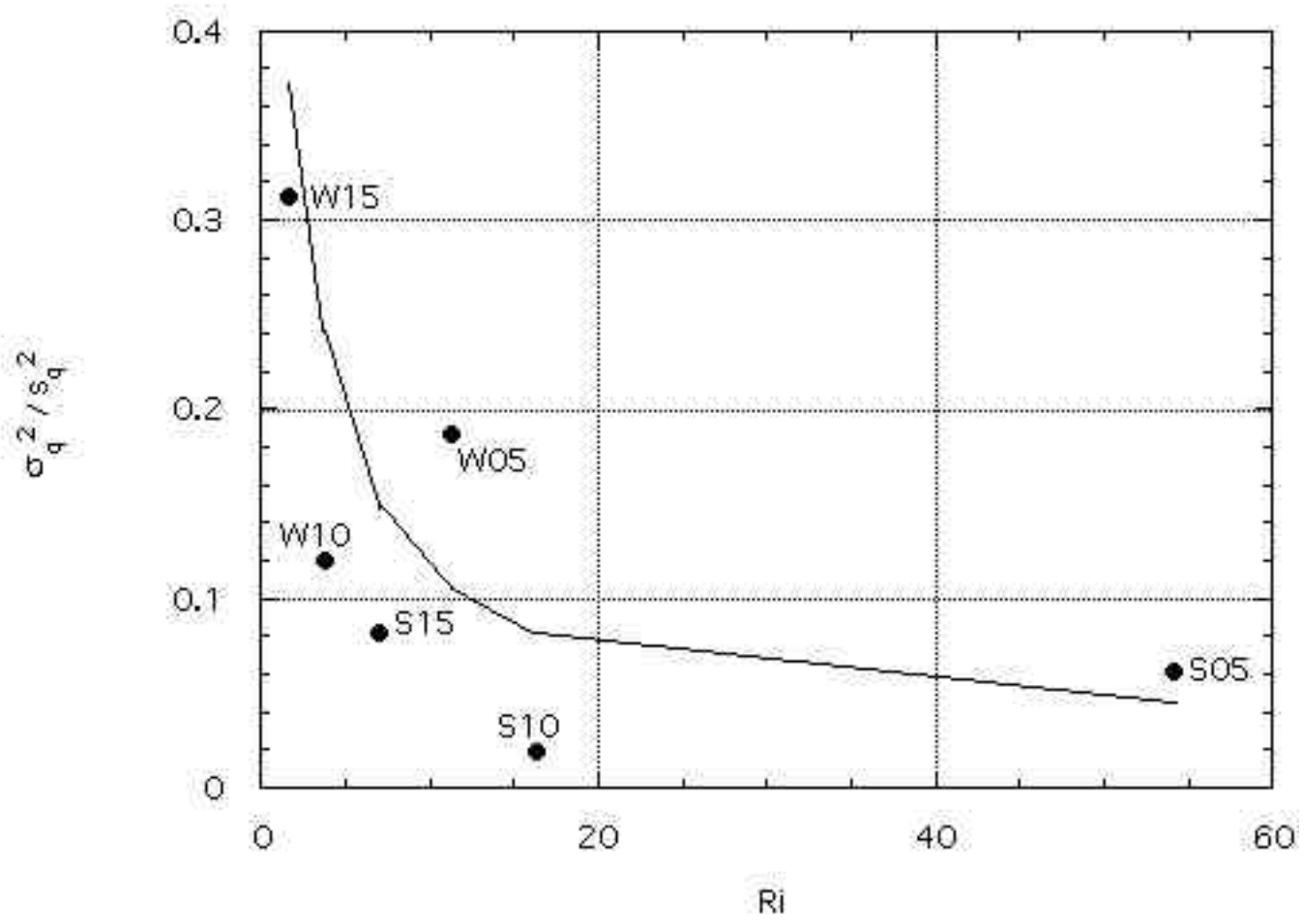
$$C_{\theta qi} (S_\theta/S_q) = \theta q (1 + c_r i) / (1 + R) / R i$$

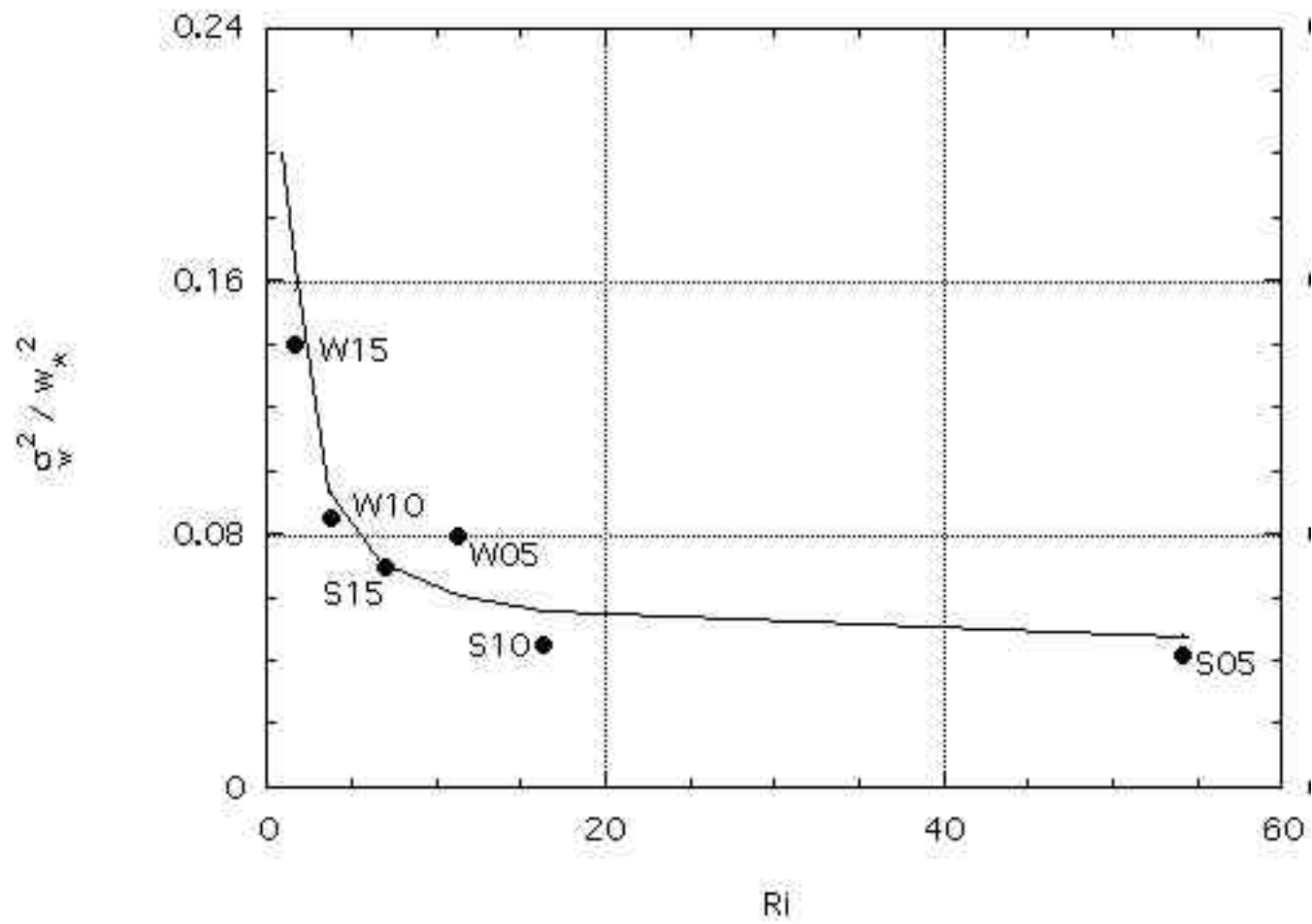
$$\sigma_{wi}^2 S_w^2 / = w (1 + c_r i) / R$$



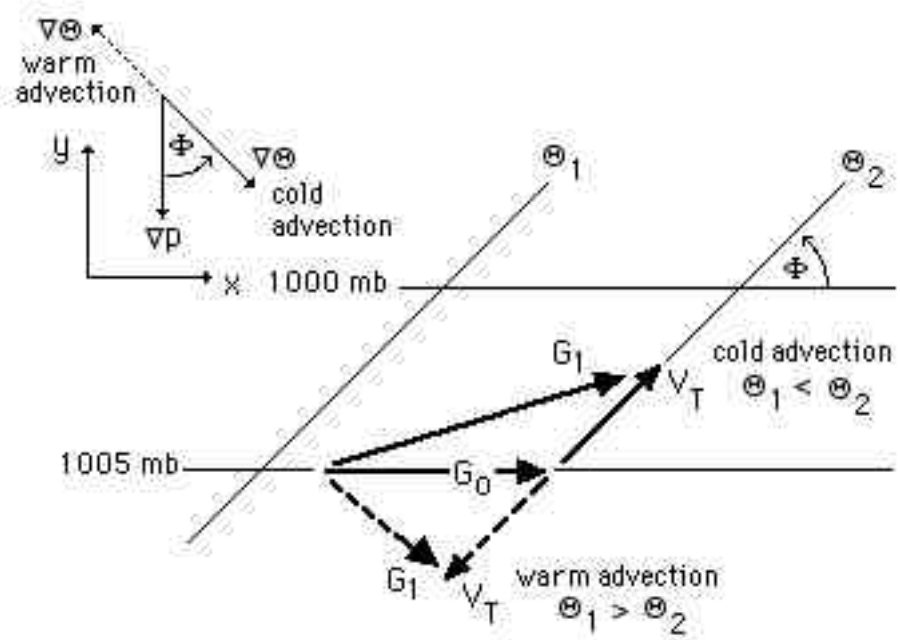


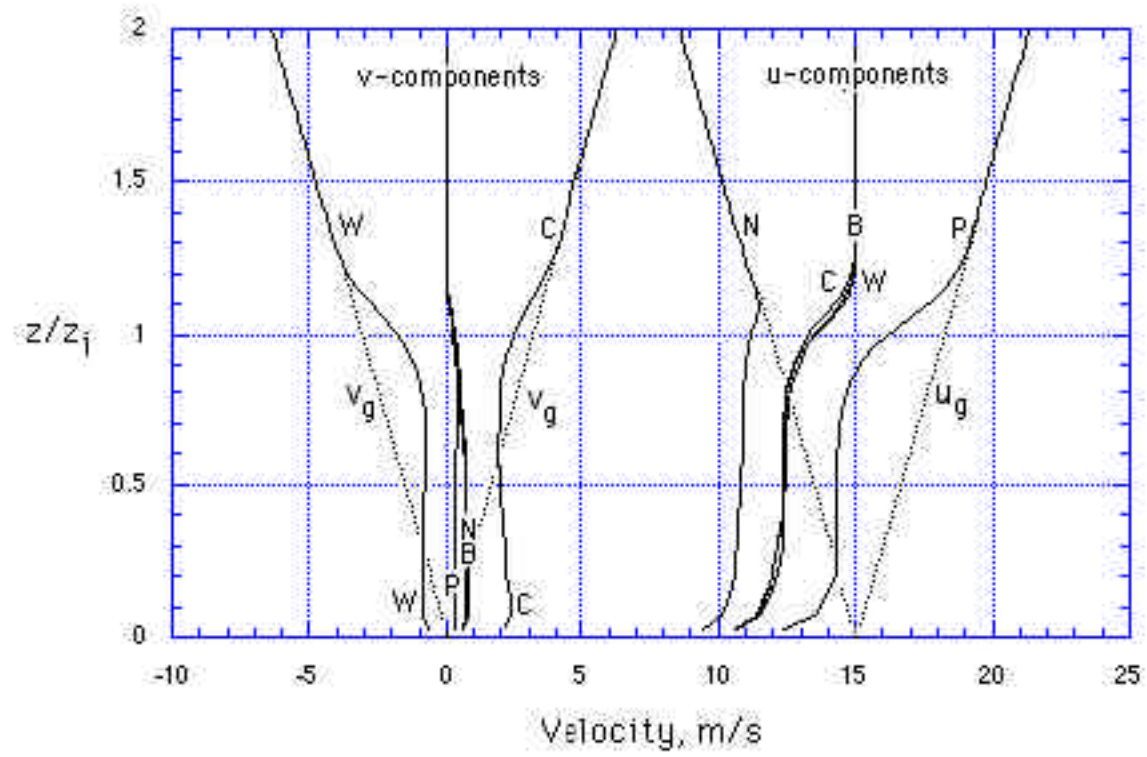


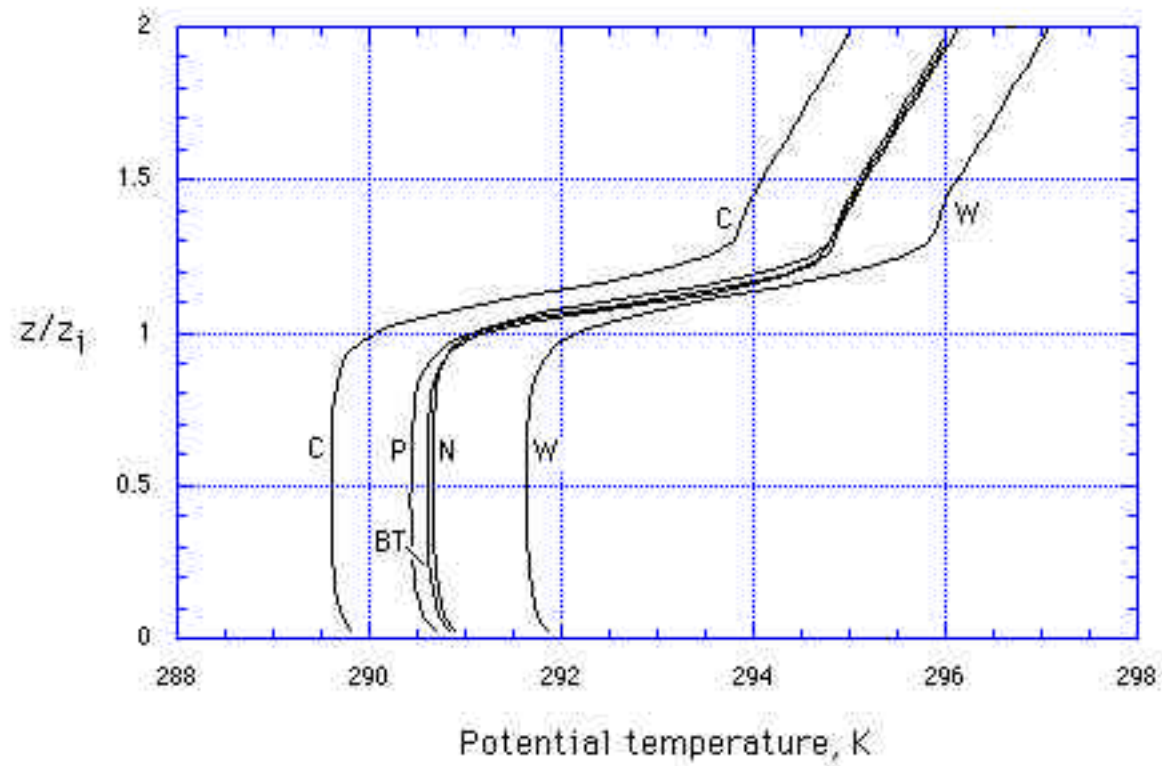


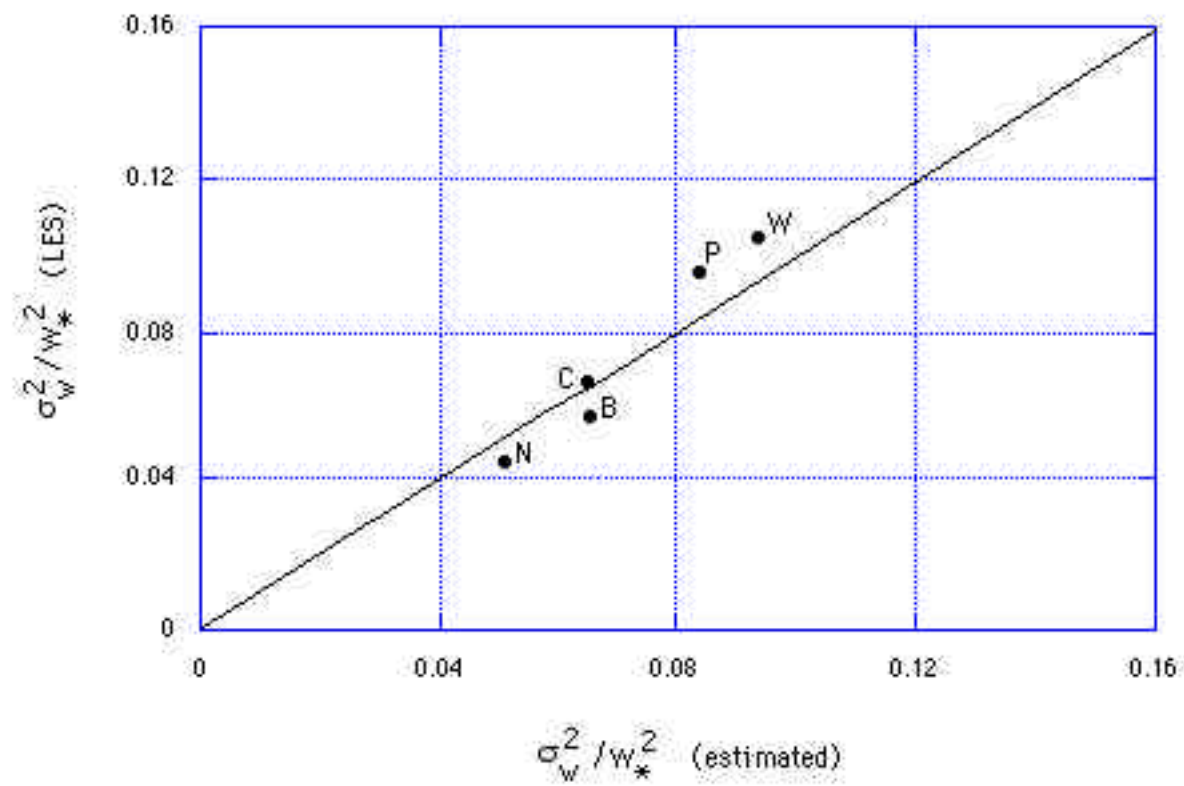


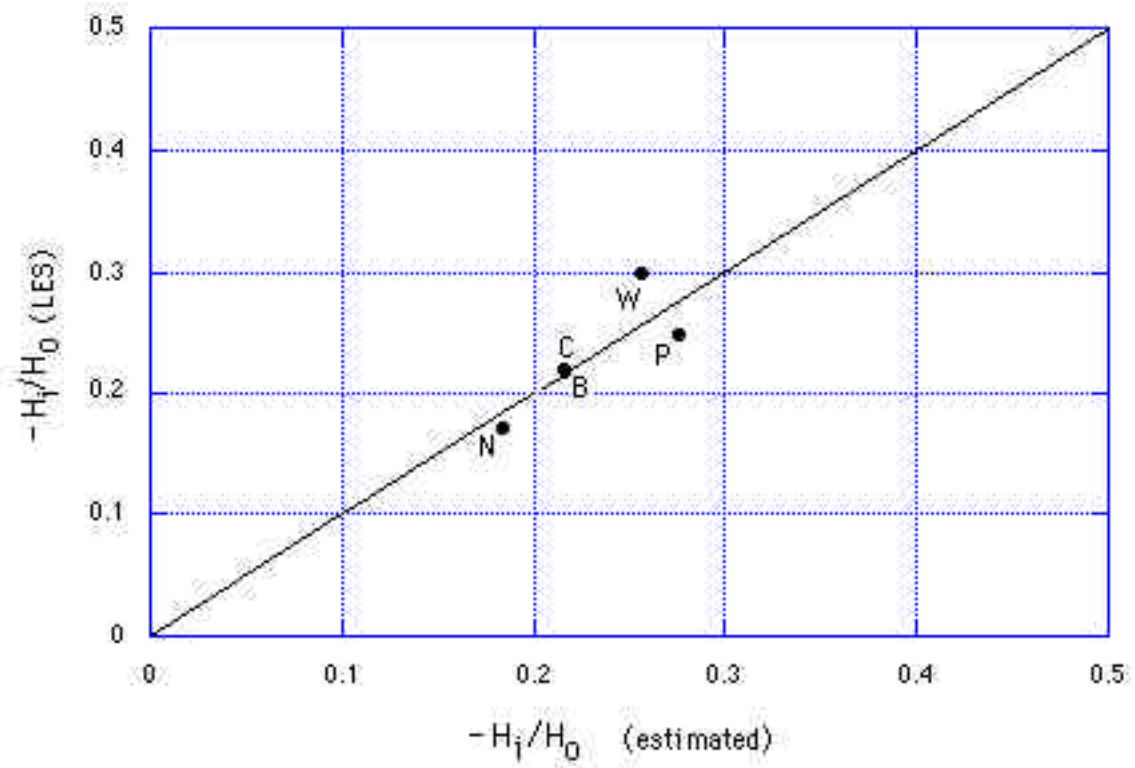
Forced convection
(baroclinic)
experiments

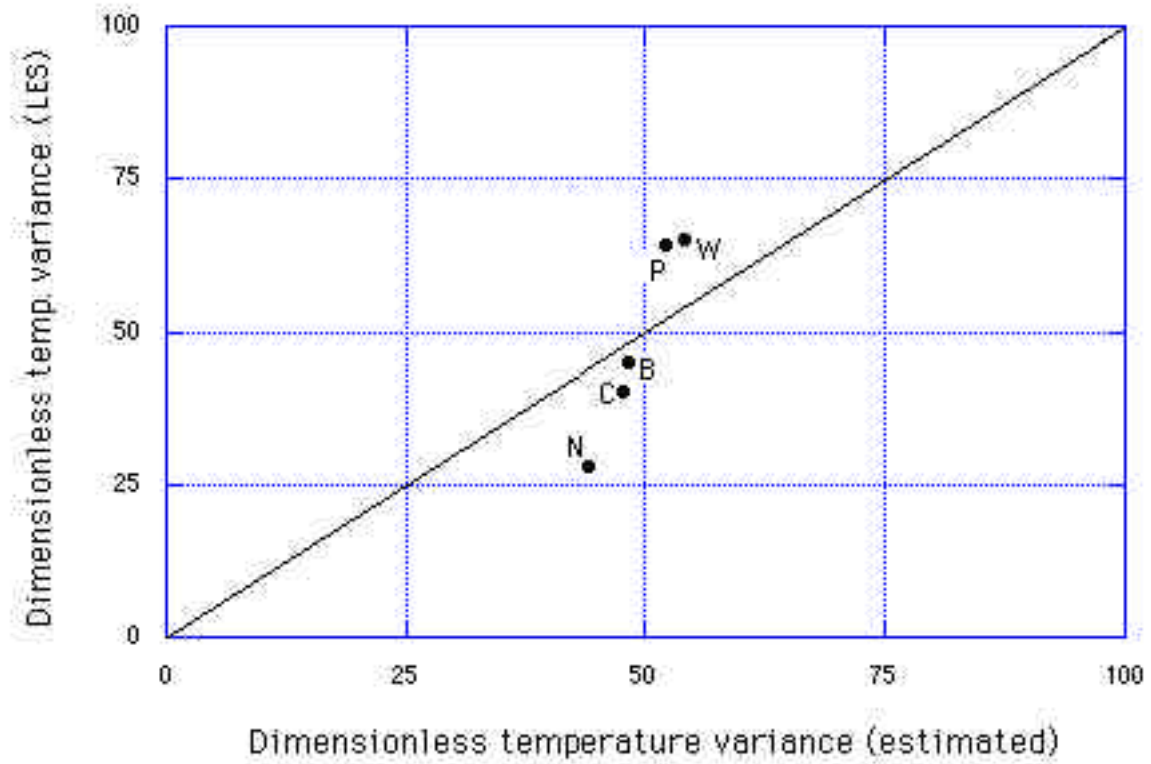












Conclusions:

- 1. Two different sets of convective scales are valid in the convective ABL (mixed layer scaling and interfacial scaling)
- 2. In the interfacial layer the characteristic (peak) values of moments are functions of the Richardson number:

$$m/S_i = C_m F_i(1/Ri)$$

- 3. Profiles of scalar variances, covariances, and gradients in the CBL can be expressed as a sum of two semi-empirical similarity functions multiplied by a combination of mixed layer scales and interfacial scales:

$$m = c_m S_m F_m(z/z_i) + C_m S_i F_i(z/z_i, 1/Ri),$$

$$H = w_* \Theta_* (1 - z/z_i) - C_H S_w S_\theta z/z_i (1 + 8 Ri)/(1 + 1/R)^{1/2}$$

$$Q = w_* q_* (1 - z/z_i) - C_Q S_w S_q z/z_i (1 + 8 Ri)/(1 + 1/R)^{1/2}$$

$$\sigma^2 = 1 \cdot \Theta_*^2 (1 - z/z_i) / (z/z_i)^{2/3} + C_\theta S_\theta^2 [(z/z_i)^9 / (2 \cdot 1 z/z_i)^9] [(1 + 8/R)/(1 + 1/R)]$$

$$\sigma_q^2 = 2 \cdot 0_*^2 q_* (1 - z/z_i) / (z/z_i)^{2/3} + C_q S_q^2 [(z/z_i)^3 / (2 \cdot 2 z/z_i)^7] [(1 + 8/R)/(1 + 1/R)]$$

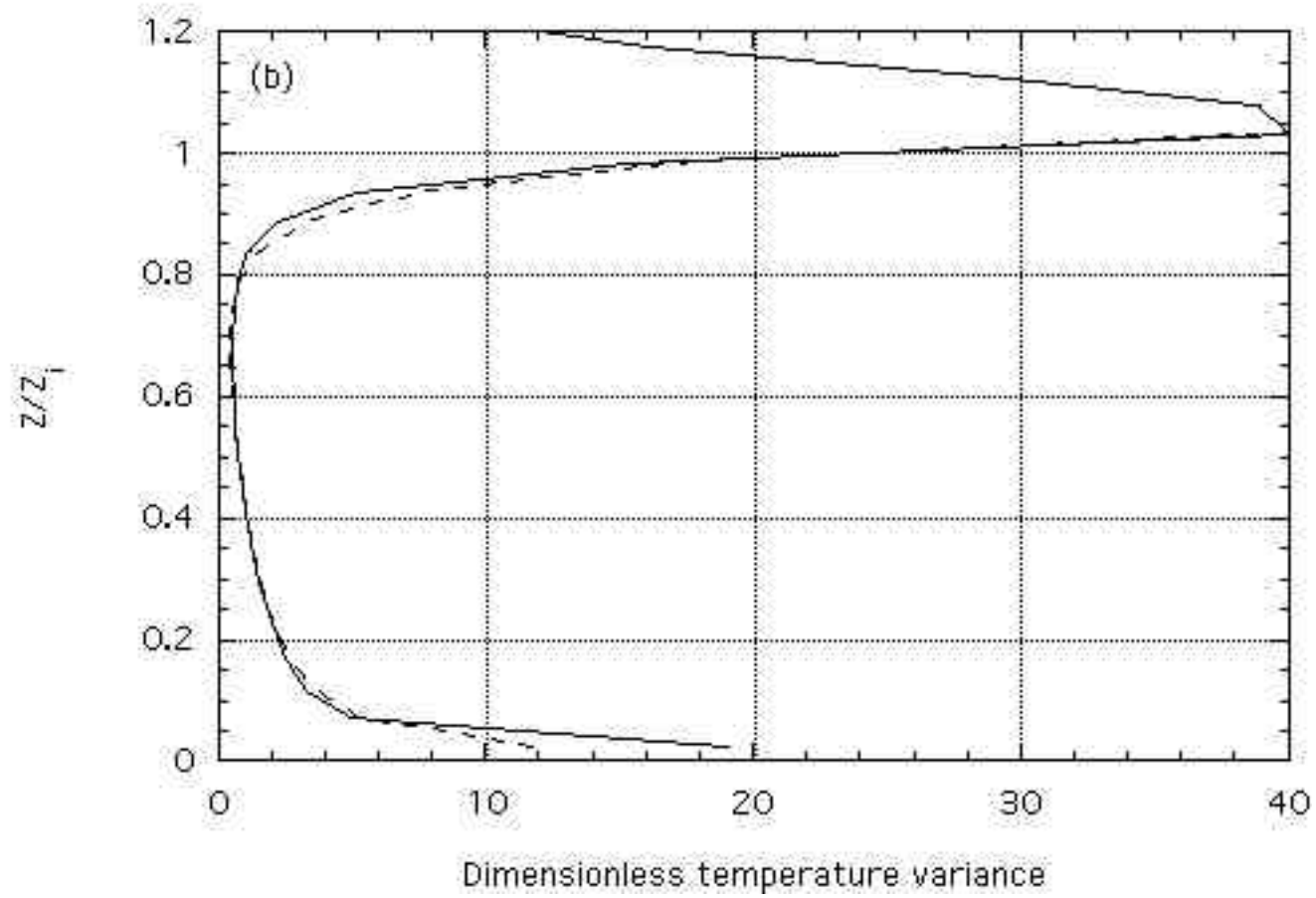
$$c_{\theta q} = 1 \cdot \Theta_* q_* (1 - z/z_i) / (z/z_i)^{2/3} + C_{\theta q} S_\theta S_q [(z/z_i)^8 / (2 \cdot 2 z/z_i)^8] [(1 + 8/R)/(1 + 1/R)]$$

$$\sigma_w^2 = 1 \cdot 4_*^2 (1 - z/z_i)^{4/3} (z/z_i)^{2/3} + C_w S_w^2 [(z/z_i)^{1/2} (1 \cdot 1 z/z_i)^{1/3}] (1 + 8/R)$$

and also

$$d\Theta/dz = -\Theta_*/z_i (1 - z/z_i)^4 / (z/z_i)^{4/3} + \gamma_i (z/z_i)^9 / (2 \cdot 2 \cdot 3 z/z_i)^9$$

$$dq/dz = -q_*/z_i (1 - z/z_i)^4 / (z/z_i)^{4/3} + g_i (z/z_i)^9 / (2 \cdot 2 \cdot 3 z/z_i)^9$$



The End

Thank you for your attention!

